



TECHNICAL MEMORANDUM

DATE January 14, 2025

Project No. 31405712.2139

TO Stephen P. Madden, Geotechnical Engineer
Vermont Agency of Transportation

CC

FROM Karen A. Roth

EMAIL karen.roth@wsp.com

**SUMMARY OF GEOTECHNICAL INVESTIGATION AND SUBSURFACE CONDITIONS
BRIDGE NO. 42, VT ROUTE 30 OVER WINHALL RIVER
JAMAICA, VERMONT
VTRANS JAMAICA ER P23-1(216)**

INTRODUCTION

WSP USA Inc. (WSP) is pleased to provide the Vermont Agency of Transportation (VTrans) with this Technical Data Memorandum summarizing our geotechnical investigation for the proposed replacement of Bridge No. 42 carrying Vermont Route 30 over the Winhall River in Jamaica, Vermont. This memorandum presents the results of the subsurface investigation we performed in November 2024, consisting of two geotechnical borings conducted at the proposed bridge abutment locations, and includes the resulting boring logs, rock core evaluations, and laboratory test results on select soil and rock samples.

This memorandum constitutes the completion of our proposed scope of work¹ submitted to VTrans on October 18, 2024 with subsequent work authorization #WA00035 dated October 24, 2024, under our On-Call Geotechnical Services Agreement with VTrans (Contract No. PS0836) dated November 1, 2020.

PROJECT BACKGROUND

The former Bridge No. 42 was constructed in 1930 and widened in 1980, and consisted of a two-span structure with concrete abutments, pier, and deck.^{2,3} Based on discussion with VTrans, WSP understands that in the July 2023 flood event, the former bridge was damaged and subsequently fully removed, including the abutments, and riprap slope protection was placed at the site of the former abutments. A temporary off-alignment structure was installed to the north of the former bridge and currently carries VT Rt. 30 traffic over the river. Based on the

¹ WSP USA Inc. Proposal for Geotechnical Borings: Bridge 42, VT Route 30, Jamaica, Vermont, VTrans Jamaica ER P23-1(216). Proposal No. 2024US312139, dated October 18, 2024.

² State of Vermont Department of Highways. Record Plans: Proposed Improvement Bridge Project, Town of Jamaica, County of Windham, Route No. Vt. Rte. 30, Bridge No. 42. Contract dated June 25, 1979; construction accepted September 10, 1980.

³ VTrans. Bridge 42 Inspection Report. Inspection date August 24, 2023.

preliminary plans⁴ provided by VTrans, we understand that VTrans proposes to construct a replacement Bridge 42 on-alignment at the site of the former bridge.

GEOLOGIC SETTING

Regional Surficial Geology

The surficial geology of the bridge site is mapped as a glaciofluvial outwash deposit consisting of horizontally-bedded gravel. The outwash may be overlain in some areas by a thin veneer of postglacial alluvium. Regional mapping indicates that the outwash is underlain by glacial till mantling the bedrock.⁵

Regional Bedrock Geology

The bedrock beneath the bridge site is mapped as Middle and Early Mesoproterozoic (i.e., Precambrian) rocks of the Washington Gneiss and Wilcox Formation, previously mapped as the Mount Holly Complex. The lithology is described as dark- to light-gray, heterogeneous, well-layered, biotite-quartz-plagioclase gneiss, containing variable amounts of magnetite, hornblende, and garnet, with little potassium feldspar. The parent, premetamorphic lithologies (i.e., protoliths) may have been volcanoclastic and clastic sediments.⁶

SUBSURFACE INVESTIGATION

WSP subcontracted Seaboard Drilling, LLC (Seaboard) of Somersworth, NH to perform the two (2) borings shown in Figure 1. The borings, designated as B425 and B545, were completed between November 19, 2024 and November 21, 2024. Seaboard completed the borings using a Mobile B-53 truck-mounted drill rig and drive-and-wash drilling methods with 4-inch inside diameter (I.D.) casing.

Standard penetration testing (SPT) was performed at 5-foot intervals using a calibrated automatic hammer system and a standard 2-inch split spoon sampler in general accordance with ASTM D1586. For each SPT location, the split spoon sampler was driven 24 inches with a 140-pound automatic hammer dropped 30 inches, and WSP recorded the number of hammer blows required to advance the sampler through each 6-inch increment. Measured, uncorrected N-values, calculated as the sum of the hammer blows to advance the sampler during the 6-inch to 18-inch interval, are provided in the boring logs in Appendix A. The hammer correction factor of 1.55 shown on the boring logs was obtained from the hammer calibration report⁷ provided by Seaboard. WSP collected and stored soil samples in sealed glass jars for later evaluation and laboratory testing.

Each boring was advanced to the top of bedrock, after which 15 feet of rock core was collected in B425 and 10 feet of rock core was collected in B545 using an NQ-size 1.88-inch I.D. diamond-tipped core barrel. The rock core samples were placed in wooden boxes and transported to the WSP office in Merrimack, NH. Total Core Recovery (TCR), calculated Rock Quality Designation (RQD), and coring rates were recorded for each core run and are provided on the boring logs in Appendix A.

⁴ VTrans. Preliminary Plans: Proposed Improvement Bridge Project, Town of Jamaica, County of Windham, Route No. Vermont Route 30 (Minor Arterial), Bridge No. 42. Dated May 21, 2024.

⁵ Stewart, D.P. and MacClintock, P., 1970. Surficial Geologic Map of Vermont. Vermont Geological Survey, 1 plate, scale 1:250,000.

⁶ Ratcliffe, N.M., Stanley, R.S., Gale, M.H., Thompson, P.J., and Walsh, G.J., 2011. Bedrock Geologic Map of Vermont, U.S. Geological Survey Scientific Investigations Map 3184, 3 sheets, scale 1:100,000.

⁷ Geosciences Testing and Research, Inc. Standard Penetration Test Energy Measurement Calibration, Mobile Truck B-53 Drill Rig - Automatic Hammer (S/N 2127), Chicopee, MA 01013. Dated March 7, 2024.

WSP's field engineer monitored drilling activities, logged the subsurface conditions encountered, and obtained soil samples and rock core for use in visual description and classification and subsequent laboratory testing. Boring logs, including details of the sampling methods used, field data obtained, soil and rock conditions encountered during the investigation, bedrock lithologic conditions, and borehole backfilling details, are provided in Appendix A. An explanation of the boring log symbols and terms used for the soil and rock descriptions precedes the boring logs. A detailed summary of the rock core quality parameters from the recovered rock core is presented in Table 2 and photographs of the rock core are presented in Appendix B. The as-drilled boring locations are shown on Figure 1 and are based on survey files provided to WSP by VTrans.

LABORATORY TESTING PROGRAM

GeoTesting Express (GTX) of Acton, MA performed soil and rock laboratory testing that included index and classification testing of representative SPT soil samples and uniaxial compressive strength testing of representative rock core samples in accordance with applicable American Association of State Highway Transportation Officials (AASHTO) and American Society of Testing and Material (ASTM) testing procedures. The types and quantities of laboratory tests conducted are summarized in Table 1. Table 3 (attached) and Table 4 (attached) provide summaries of the laboratory testing results. Laboratory testing results are also summarized on the boring logs in Appendix A and are provided in full in Appendix C.

Table 1: Laboratory Testing Summary of Soil and Rock

Laboratory Test	Material	Test Standard	No. Tests Completed
Grain Size (Sieve)	Soil	ASTM D6913	11
Moisture Content	Soil	ASTM D2216	11
Unconfined Compressive Strength	Rock	ASTM D7012C	4

SUBSURFACE CONDITIONS

The boring logs in Appendix A provide detailed descriptions of the soil, bedrock, and measured groundwater conditions encountered in the borings. Soils include topsoil, asphalt interpreted as the base pavement of the former bridge approach, fill materials placed during construction of the former bridge, and glacial deposits, including glaciofluvial outwash and glacial till, overlying bedrock. The following descriptions summarize the major stratigraphic units from the existing ground surface to depth.

Topsoil: Topsoil was encountered in both borings; the thickness of the topsoil ranged from 0.5 inch to 1 inch. The topsoil generally consisted of silty fine sand with roots and grass.

Base Pavement of Former Bridge Approach: A layer of gravel with broken asphalt, interpreted as the base pavement of the former bridge approach roadway, was encountered in both borings directly below the topsoil. The thickness ranged from 3 inches to 6 inches. The layer generally consisted of dense, fine to coarse gravel with some sand and trace fines. Laboratory classifications generally described the layer as A-1-a (AASHTO classification) and GP or SW (USCS classification).

Fill: A layer interpreted as granular fill was encountered beneath the base pavement in both borings. The approximate fill thickness ranged from 4 feet to 10 feet. The fill generally consisted of medium dense to very dense, fine to coarse gravel with sand fractions ranging from “some” to “sandy” and little fines. Laboratory classifications generally described the layer as A-1-b (AASHTO classification) and SM or SP-SM (USCS classification). Uncorrected N-values for the fill in these borings ranged from 26 to 96, with an average of 55. The fill layer overlies the glaciofluvial outwash layer, transitioning at a depth of 10 feet bgs in B425 and 5 feet bgs in B545.

Glaciofluvial Outwash: A layer interpreted as glaciofluvial outwash deposits was encountered beneath the fill in both borings. The approximate layer thickness ranged from 13 feet to 16 feet. The glaciofluvial outwash was variable and generally consisted of medium dense to very dense, fine to medium sand with little to some fines and trace to little gravel; or dense, fine to coarse gravel with some sand and little fines; or hard non-plastic silt with sand fractions ranging from “some” to “sandy” and trace gravel. Laboratory classifications generally described the layer as A-2-4, A-1-a, or A-4 (AASHTO classification) and SM or ML (USCS classification). Uncorrected N-values for the glaciofluvial outwash in these borings ranged from 25 to refusal, with an average of 54. The glaciofluvial outwash layer overlies glacial till layer, transitioning at a depth of 23 feet bgs in B425 and 21 feet bgs in B545.

Glacial Till: A layer interpreted as glacial till was encountered beneath the glaciofluvial outwash in both borings. The approximate glacial till thickness ranged from 7 feet to 11 feet. The glacial till generally consisted of very dense fine to coarse sand and gravel with silt fractions ranging from “some” to “silty”. Cobbles and boulders were observed in this layer during drilling. Laboratory classifications generally described the layer as A-4 or A-1-b (AASHTO classification) and GM or SM (USCS classification). SPT sampling within the glacial till encountered refusal for all samples. The glacial till layer overlies bedrock, transitioning at a depth of 29.5 feet bgs in B425 and 32 feet bgs in B545.

Bedrock: The weathered bedrock surface was encountered at 29.5 feet bgs in B425 and 32.0 feet bgs in B545; the competent bedrock surface was encountered at 31.1 ft bgs in B425 and 35.5 ft bgs in B545. 15 feet of rock core was collected in B425 and 10 feet of rock core was collected in B545 in 5-foot runs. The bedrock collected in these borings generally consists of gray, fine- to medium-grained, medium strong to very strong (R3-R5, ISRM classification⁸), fresh to slightly weathered (W1-W2, ISRM classification⁸), biotite-quartz gneiss with Rock Quality Designations (RQD) ranging from 8% to 56% with an average of 33%. The Rock Mass Rating⁹ (RMR), a measure of overall rock mass conditions, ranges from 35 to 58 with an average of 46. The RMR is a geo-mechanical classification system for design and construction of rock excavation such as tunnels, mines, slopes, and foundations, using field estimates and laboratory measurements of compressive strength, and field observations of discontinuity spacing, discontinuity condition, groundwater, and discontinuity orientation. A Geological Strength Index¹⁰ (GSI) value of 55 was interpreted for the rock encountered in the borings. The GSI provides a system for estimating the reduction in rock mass strength under different geological conditions, using field observations of rock mass structure and discontinuity condition. Table 2 contains a detailed summary of the data generated from the rock coring and core logging.

⁸ Wyllie, D.C. and Mah, C.W., 2004. Rock Slope Engineering: Civil and Mining, 4th ed., Spon Press, London, p. 381-397, Appendix II: Quantitative Description of Discontinuities in Rock Masses (includes International Society of Rock Mechanics [ISRM] procedures).

⁹ Bieniawski, Z.T., 1989. Engineering Rock Mass Classifications, John Wiley & Sons, NY.

¹⁰ Marinos, P. and Hoek, E. 2000. GSI: a geologically friendly tool for rock mass strength estimation. ISRM International Symposium, Melbourne, Australia, paper number ISRM-IS-2000-035.

Groundwater: WSP measured groundwater levels in boring B545 during drilling. Measurements were made with temporary steel casing in the ground upon completion of rock coring. The groundwater level was measured at 13.5 feet bgs (elevation 1206.9 feet) in B545, which is consistent with the Winhall River elevation. We note that groundwater levels will vary seasonally from that measured.

CLOSING AND LIMITATIONS

WSP prepared this Technical Memorandum for the exclusive use of VTrans for specific application to the replacement of Bridge No. 42 carrying VT Rt. 30 over the Winhall River in Jamaica, Vermont. We performed the geotechnical site investigation and compiled our subsurface conditions summary in accordance with generally accepted soil engineering practices in this geographical area and under similar time and financial constraints. Our interpretations are based, in part, on information obtained from the referenced subsurface explorations completed at the discrete locations described in the memorandum. Variations in the nature and extent of subsurface conditions between explorations should be expected. WSP makes no other warranty, either express or implied.

The professional services provided by WSP for this project include only the geotechnical aspects of the subsurface conditions at this site. The presence or implications of possible surface and/or subsurface contamination resulting from previous activities or uses of the site and/or resulting from the introduction onto the site of materials from off-site sources are outside the terms of reference for this report and have not been investigated or addressed.

WSP appreciates the opportunity to provide our geotechnical services to VTrans for this project. Please contact us if you have any questions.

Sincerely,

WSP USA, Inc.



Karen A. Roth
Senior Consultant, Geotechnical Engineering



Jeffrey D. Lloyd, PE
Assistant Vice President, Geotechnical Engineering

KAR/LMP/JDL

Distribution: Melissa E. Landon, PhD, PE, Lead Consultant, Geotechnical Engineering

Attachments: Table 1: Laboratory Testing Summary of Soil and Rock (in text)
Table 2: Summary of Rock Core Quality
Table 3: Summary of Soil Index and Classification Laboratory Testing Results
Table 4: Summary of Rock Laboratory Testing Results

Figure 1: Boring Location Plan

Appendix A: Boring Logs
Appendix B: Rock Core Photographs
Appendix C: Laboratory Test Results

[https://wsponlinenam.sharepoint.com/sites/us-vtrans-jamaica-er/shared documents/06 deliverables/final report 01-14-2025/31405712.2139 vtrans jamaica geotechnical data memorandum.docx](https://wsponlinenam.sharepoint.com/sites/us-vtrans-jamaica-er/shared%20documents/06%20deliverables/final%20report%2001-14-2025/31405712.2139%20vtrans%20jamaica%20geotechnical%20data%20memorandum.docx)

Tables

Table 2: Summary of Rock Core Quality
Bridge 42, VT Route 30
VTrans Jamaica ER P23-1(216)
Jamaica, VT

Test Boring Designation	Core Size	Run						TCR ¹		RQD ²		Physical Rock Parameters				Lithologic, Rock Mass and Discontinuity Description ^{5,6}
		No.	Midpoint Depth Below Bedrock Surface (ft)	Depth Below Ground Surface (ft)			Length (ft)	Length (ft)	%	Length (ft)	%	Designation	Weathering ³	Estimated Field Strength ³	Rock Mass Rating [RMR] ⁴	
				Start	End	Midpoint										
B425	NQ (1.88)	R1	3.0	30.0	35.0	32.5	5.0	3.9	77%	0.40	8%	Very Poor	Slightly Weathered (W2) to Completely Weathered (W5)	Medium Strong (R3)	35	Medium gray, fine- to medium-grained, medium strong (R3, bottom 3.9 ft), biotite-quartz GNEISS, completely weathered (W5, top 1.1 ft) to slightly weathered (W2, bottom 3.9 ft); discontinuities shallowly to moderately dipping (up to 45°), closely spaced, tight, irregular, very rough to smooth, with fine to medium sand infilling in some fractures, average 8.0 fractures per foot. Biotite and quartz banding and folding observed throughout run. [MOUNT HOLLY COMPLEX].
		R2	8.0	35.0	40.0	37.5	5.0	4.4	88%	1.55	31%	Poor	Slightly Weathered (W2)	Medium Strong (R3)	43	Brownish gray, fine- to medium-grained, medium strong (R3), biotite-quartz GNEISS, slightly weathered (W2); discontinuities shallowly to moderately dipping, very closely spaced, irregular to planar, smooth to rough, with fine sand infilling in fractures, average 5.2 fractures per foot. Biotite and quartz banding and folding observed throughout run. [MOUNT HOLLY COMPLEX].
		R3	13.0	40.0	45.0	42.5	5.0	4.3	86%	0.90	18%	Very Poor	Slightly Weathered (W2)	Strong (R4)	40	Brown (weathered) to gray, fine- to medium-grained, strong (R4), biotite-quartz GNEISS, slightly weathered (W2); discontinuities shallowly to moderately dipping (up to 45°), very closely to closely spaced, planar to irregular, smooth to rough, with fine sand infilling in fractures, average 5.4 fractures per foot. Biotite and quartz banding observed throughout run. [MOUNT HOLLY COMPLEX].
B545	NQ (1.88)	R1	5.7	35.2	40.2	37.7	5.0	4.7	93%	2.80	56%	Fair	Fresh (W1) to Completely Weathered (W5)	Very Strong (R5)	54	White to light and dark gray, fine-grained, very strong (R5), micaceous GNEISS, completely weathered (W5, top 0.3 ft) to fresh (W1); discontinuities shallowly to horizontally dipping, very closely spaced, planar to irregular, smooth to rough, average 3.2 fractures per foot. Alternating white and light or dark gray banding 0.1-0.4 mm thick observed throughout run. Quartz vein 10 mm thick at 39 ft bgs. [MOUNT HOLLY COMPLEX].
		R2	10.7	40.2	45.2	42.7	5.0	5.0	100%	2.60	52%	Fair	Fresh (W1) to Slightly Weathered (W2)	Very Strong (R5)	58	White to light and dark gray, fine-grained, very strong (R5), GNEISS, fresh (W1) to slightly weathered (W2); discontinuities shallowly to steeply dipping, very closely spaced, planar to stepped, smooth to rough, average 4.4 fractures per foot. Mica, biotite, and quartz banding and folding observed throughout run. [MOUNT HOLLY COMPLEX].

Notes:

1. TCR = total core recovery. Total core recovery is the length of core recovered divided by the length of the run.
2. RQD = rock quality designation. RQD is the total length of intact, full diameter core pieces recovered with a length greater than or equal to 4 inches measured along the core axis. The percent RQD is the total length of RQD measured divided by the run length. Note that vertical discontinuities are not included in determination of RQD.
3. Weathering and Estimated Field Strength based on Tables II.4 and II.3 (respectively) in Wyllie and Mah, 2004, Rock Slope Engineering: Civil and Mining, 4th Edition (based on ISRM, 1981).
4. Rock Mass Rating (RMR) System (Bieniawski, 1989) assigns numerical ratings to six parameters, including the strength of the intact rock, the RQD, the discontinuity spacing, groundwater conditions, and orientation of discontinuities. These ratings are summed to provide the RMR value. The rating adjustment for joint orientation was assigned a value of 0; correlation of geologic field mapping data of exposed rock outcrops with the rock core samples and proposed foundation type may allow for a different rating adjustment for joint orientation, and thus a modification to the RMR value shown on this table.
5. Bedrock formation name from: Ratcliffe, N.M., Stanley, R.S., Gale., M.H., Thompson, P.J., and Walsh, G.J., 2011, Bedrock geologic map of Vermont: U.S. Geological Survey Scientific Investigations Map 3184, 3 sheets, scale 1:100,000.
6. ft = feet, in = inches
- Prepared by: LMP
Checked by: KAR
Reviewed by: JDL

Table 3: Summary of Soil Index and Classification Laboratory Testing Results
Bridge 42, VT Route 30
VTrans Jamaica ER P23-1(216)
Jamaica, VT

Test Boring Designation ¹	Ground Surface Elevation (feet) ²	Sample Number ³	Sample Depth Below Ground Surface (feet)	Approximate Sample Elevation (feet) ²	Laboratory Testing ^{3,4,5}		Soil Classification	
					Sieve Minus No. 200 ⁴ (%)	Moisture Content ⁵ (%)	AASHTO ^{6,7}	USCS ^{6,7}
B425	1213.5	S1B	0.3 - 2.0	1213.3 - 1211.5	15.8	5.6	A-1-b	SM
		S2	5.0 - 7.0	1208.5 - 1206.5	17.8	5.7	A-1-b	SM
		S4	15.0 - 17.0	1198.5 - 1196.5	64.4	17.2	A-4	ML
		S5	20.0 - 22.0	1193.5 - 1191.5	65.2	22.1	A-4	ML
		S6	25.0 - 25.4	1188.5 - 1188.2	37.7	13.2	A-4	GM
B545	1220.4	S1A	0.1 - 0.6	1220.3 - 1219.8	3.9	2.1	A-1-a	SW
		S1B	0.6 - 2.0	1219.8 - 1218.4	10.7	2.6	A-1-b	SP-SM
		S2	5.0 - 7.0	1215.4 - 1213.4	13.3	9.2	A-1-a	SM
		S3	10.0 - 12.0	1210.4 - 1208.4	51.2	17.8	A-4	ML
		S4	15.0 - 15.8	1205.4 - 1204.5	38.4	13.7	A-4	SM
		S7	25.0 - 25.3	1195.4 - 1195.0	36.7	13.1	A-4	SM

Notes:

1. Boring locations are illustrated in Figure 1: Boring Location Plan of the Geotechnical Data Memorandum.
2. The as-drilled boring elevations are derived from electronic file "x24b002sv.dgn" provided to WSP by VTrans on December 18, 2024.
3. Laboratory testing was performed by Geotesting Express of Acton, MA.
4. Particle size testing was performed in accordance with ASTM D6913, Standard Test Methods for Particle-Size Distribution (Gradation) of Soils Using Sieve Analysis.
5. Moisture content testing was performed in accordance with ASTM D2216, Standard Test Methods for Laboratory Determination of Water (Moisture) Content of Soil and Rock by Mass.
6. AASHTO and USCS symbols were assigned based on interpreted laboratory test results provided by Geotesting Express on December 13, 2024.
7. Complete laboratory test results for soil testing are provided in Appendix C.

Prepared By: LMP
 Checked By: KAR
 Reviewed By: JDL

Table 4: Summary of Rock Laboratory Testing Results
Bridge 42, VT Route 30
VTrans Jamaica ER P23-1(216)
Jamaica, VT

Test Boring Designation ¹	Ground Surface Elevation ² (ft)	Top of Bedrock Depth ³ (ft)	Top of Bedrock Elevation (ft)	Sample Number ⁴ (-)	Sample Depth Below Top of Bedrock (ft)	Sample Depth Below Ground Surface (ft)	Sample Elevation (ft)	Unconfined Compressive Strength ⁵	Bulk Density ⁶
								(psi)	(pcf)
B425	1213.5	29.5	1184.0	Run 2	7.2 - 7.6	36.7 - 37.1	1176.8 - 1176.5	6,844	168
B425	1213.5	29.5	1184.0	Run 3	14.1 - 14.5	43.6 - 44.0	1169.9 - 1169.5	10,660	169
B545	1220.4	32.0	1188.4	Run 1	6.5 - 6.9	38.5 - 38.9	1181.8 - 1181.5	15,924	166
B545	1220.4	32.0	1188.4	Run 2	12.2 - 12.6	44.2 - 44.6	1176.1 - 1175.8	20,093	167

Notes:

1. Boring locations are illustrated in Figure 1: Boring Location Plan of the Geotechnical Data Memorandum.
2. The as-drilled boring elevations are derived from electronic file "x24b002sv.dgn" provided to WSP by VTrans on December 18, 2024.
3. Top of bedrock surface refers to the interpreted top of weathered bedrock based on roller cone resistance or material observed in wash cuttings. Notes regarding weathered rock are provided in Appendix A.
4. Laboratory testing was performed by Geotesting Express (GTX) of Acton, MA.
5. Testing was performed based on ASTM D7012 Method C - Standard Test Methods for Uniaxial Compressive Strength of Intact Rock Core Specimens.
7. Density determined by GTX on core samples by measuring dimensions and weight and then calculating.
8. Complete laboratory test results for rock core testing are provided in Appendix C.
9. ft = feet; psi = pounds per square inch; pcf = pounds per cubic foot

Prepared By: LMP
 Checked By: KAR
 Reviewed By: JDL

Figure



<

APPENDIX A

Boring Logs

Table A-1

UNIFIED SOIL CLASSIFICATION SYSTEM					TERMS DESCRIBING DENSITY/CONSISTENCY																														
MAJOR DIVISIONS			GROUP SYMBOLS	TYPICAL NAMES																															
COARSE-GRAINED SOILS (more than half of material is larger than No. 200 sieve size)	GRAVELS (more than half of coarse fraction is larger than No. 4 sieve size)	CLEAN GRAVELS	GW	Well-graded gravels, gravel-sand mixtures, little or no fines.	Coarse-grained soils (more than half of material is larger than No. 200 sieve): Includes (1) clean gravels; (2) silty or clayey gravels; and (3) silty, clayey or gravelly sands. Consistency is rated according to standard penetration resistance. Modified Burmister System <table><tr><th>Descriptive Term</th><th>Portion of Total</th></tr><tr><td>trace</td><td>0% - 10%</td></tr><tr><td>little</td><td>11% - 20%</td></tr><tr><td>some</td><td>21% - 35%</td></tr><tr><td>adjective (e.g. sandy, clayey)</td><td>36% - 50%</td></tr></table> <table><tr><th>Density of Cohesionless Soils</th><th>Standard Penetration Resistance N-Value (blows per foot)</th></tr><tr><td>Very loose</td><td>0 - 4</td></tr><tr><td>Loose</td><td>5 - 10</td></tr><tr><td>Medium Dense</td><td>11 - 30</td></tr><tr><td>Dense</td><td>31 - 50</td></tr><tr><td>Very Dense</td><td>> 50</td></tr></table>				Descriptive Term	Portion of Total	trace	0% - 10%	little	11% - 20%	some	21% - 35%	adjective (e.g. sandy, clayey)	36% - 50%	Density of Cohesionless Soils	Standard Penetration Resistance N-Value (blows per foot)	Very loose	0 - 4	Loose	5 - 10	Medium Dense	11 - 30	Dense	31 - 50	Very Dense	> 50					
		Descriptive Term	Portion of Total																																
		trace	0% - 10%																																
	little	11% - 20%																																	
	some	21% - 35%																																	
	adjective (e.g. sandy, clayey)	36% - 50%																																	
Density of Cohesionless Soils	Standard Penetration Resistance N-Value (blows per foot)																																		
Very loose	0 - 4																																		
Loose	5 - 10																																		
Medium Dense	11 - 30																																		
Dense	31 - 50																																		
Very Dense	> 50																																		
(little or no fines)	GP	Poorly-graded gravels, gravel sand mixtures, little or no fines.																																	
GRAVEL WITH FINES (Appreciable amount of fines)	GM	Silty gravels, gravel-sand-silt mixtures.																																	
	GC	Clayey gravels, gravel-sand-clay mixtures.																																	
SANDS (more than half of coarse fraction is smaller than No. 4 sieve size)	CLEAN SANDS	SW	Well-graded sands, gravelly sands, little or no fines																																
	(little or no fines)	SP	Poorly-graded sands, gravelly sand, little or no fines.																																
	SANDS WITH FINES (Appreciable amount of fines)	SM	Silty sands, sand-silt mixtures																																
		SC	Clayey sands, sand-clay mixtures.																																
FINE-GRAINED SOILS (more than half of material is smaller than No. 200 sieve size)	SILTS AND CLAYS (liquid limit less than 50)	ML	Inorganic silts and very fine sands, rock flour, silty or clayey fine sands, or clayey silts with slight plasticity.	Fine-grained soils (more than half of material is smaller than No. 200 sieve): Includes (1) inorganic and organic silts and clays; (2) gravelly, sandy or silty clays; and (3) clayey silts. Consistency is rated according to shear strength as indicated. <table><tr><th>Consistency of Cohesive soils</th><th>SPT N-Value blows per foot</th><th>Approximate Undrained Shear Strength (psf)</th><th>Field Guidelines</th></tr><tr><td>Very Soft</td><td>WOH, WOR, WOP, <2</td><td>0 - 250</td><td>Fist easily Penetrates</td></tr><tr><td>Soft</td><td>2 - 4</td><td>250 - 500</td><td>Thumb easily penetrates</td></tr><tr><td>Medium Stiff</td><td>5 - 8</td><td>500 - 1000</td><td>Thumb penetrates with moderate effort</td></tr><tr><td>Stiff</td><td>9 - 15</td><td>1000 - 2000</td><td>Indented by thumb with great effort</td></tr><tr><td>Very Stiff</td><td>16 - 30</td><td>2000 - 4000</td><td>Indented by thumbnail</td></tr><tr><td>Hard</td><td>>30</td><td>over 4000</td><td>Indented by thumbnail with difficulty</td></tr></table>				Consistency of Cohesive soils	SPT N-Value blows per foot	Approximate Undrained Shear Strength (psf)	Field Guidelines	Very Soft	WOH, WOR, WOP, <2	0 - 250	Fist easily Penetrates	Soft	2 - 4	250 - 500	Thumb easily penetrates	Medium Stiff	5 - 8	500 - 1000	Thumb penetrates with moderate effort	Stiff	9 - 15	1000 - 2000	Indented by thumb with great effort	Very Stiff	16 - 30	2000 - 4000	Indented by thumbnail	Hard	>30	over 4000	Indented by thumbnail with difficulty
		Consistency of Cohesive soils	SPT N-Value blows per foot					Approximate Undrained Shear Strength (psf)	Field Guidelines																										
		Very Soft	WOH, WOR, WOP, <2					0 - 250	Fist easily Penetrates																										
	Soft	2 - 4	250 - 500					Thumb easily penetrates																											
	Medium Stiff	5 - 8	500 - 1000					Thumb penetrates with moderate effort																											
	Stiff	9 - 15	1000 - 2000					Indented by thumb with great effort																											
Very Stiff	16 - 30	2000 - 4000	Indented by thumbnail																																
Hard	>30	over 4000	Indented by thumbnail with difficulty																																
CL	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays, lean clays.																																		
OL	Organic silts and organic silty clays of low plasticity.																																		
SILTS AND CLAYS (liquid limit greater than 50)	MH	Inorganic silts, micaceous or diatomaceous fine sandy or silty soils, elastic silts.																																	
	CH	Inorganic clays of high plasticity, fat clays.																																	
	OH	Organic clays of medium to high plasticity, organic silts.																																	
	HIGHLY ORGANIC SOILS	Pt	Peat and other highly organic soils.																																
Desired Soil Observations: (in this order) Color (Munsell color chart) Moisture (dry, damp, moist, wet, saturated) Density/Consistency (from above right hand side) Name (sand, silty sand, clay, etc., including portions - trace, little, etc.) Gradation (well-graded, poorly-graded, uniform, etc.) Plasticity (non-plastic, slightly plastic, moderately plastic, highly plastic) Structure (layering, fractures, cracks, etc.) Bonding (well, moderately, loosely, etc., if applicable) Cementation (weak, moderate, or strong, if applicable, ASTM D 2488) Geologic Origin (till, marine clay, alluvium, etc.) Unified Soil Classification Designation Groundwater level					Rock Quality Designation (RQD): RQD = $\frac{\text{sum of the lengths of intact pieces of core} > 100 \text{ mm}}{\text{length of core advance}}$ *Minimum NQ rock core (1.88 in. OD of core) Correlation of RQD to Rock Mass Quality <table><tr><th>Rock Mass Quality</th><th>RQD</th></tr><tr><td>Very Poor</td><td><25%</td></tr><tr><td>Poor</td><td>26% - 50%</td></tr><tr><td>Fair</td><td>51% - 75%</td></tr><tr><td>Good</td><td>76% - 90%</td></tr><tr><td>Excellent</td><td>91% - 100%</td></tr></table> Desired Rock Observations: (in this order) Color (Geological Society of America Rock Color Chart) Texture (aphanitic, fine-grained, etc.) Strength (ISRM Classification per Table A-2) Lithology (igneous, sedimentary, metamorphic, etc.) Hardness (very hard, hard, mod. hard, etc.) Weathering (fresh, very slight, slight, moderate, mod. severe, severe, etc.) Geologic discontinuities/jointing: -dip (horiz - 0-5, low angle - 5-35, mod. dipping - 35-55, steep - 55-85, vertical - 85-90) -spacing (very close - <5 cm, close - 5-30 cm, mod. close 30-100 cm, wide - 1-3 m, very wide >3 m) -tightness (tight, open or healed) -infilling (grain size, color, etc.) Formation (Waterville, Ellsworth, Cape Elizabeth, etc.) RQD and correlation to rock mass quality (very poor, poor, etc.) ref: AASHTO Standard Specification for Highway Bridges 17th Ed. Table 4.4.8.1.2A Recovery				Rock Mass Quality	RQD	Very Poor	<25%	Poor	26% - 50%	Fair	51% - 75%	Good	76% - 90%	Excellent	91% - 100%															
Rock Mass Quality	RQD																																		
Very Poor	<25%																																		
Poor	26% - 50%																																		
Fair	51% - 75%																																		
Good	76% - 90%																																		
Excellent	91% - 100%																																		
 Key to Soil and Rock Descriptions Including Boring Log Terms and Field Identification Information					Sample Container Labeling Requirements: <table><tr><td>Project Name / Town</td><td>Blow Counts</td></tr><tr><td>Boring Number</td><td>Sample Recovery</td></tr><tr><td>Sample Number</td><td>Date</td></tr><tr><td>Sample Depth</td><td>Personnel Initials</td></tr></table>				Project Name / Town	Blow Counts	Boring Number	Sample Recovery	Sample Number	Date	Sample Depth	Personnel Initials																			
Project Name / Town	Blow Counts																																		
Boring Number	Sample Recovery																																		
Sample Number	Date																																		
Sample Depth	Personnel Initials																																		

Table A-2**Classification of Rock Material Strengths¹**

Grade	Description	Field Identification	Approx. Range of Uniaxial Compressive Strength	
			MPa	psi
S1	Very soft clay	Easily penetrated several inches by fist	<0.025	<4
S2	Soft clay	Easily penetrated several inches by thumb	0.025-0.05	4-7
S3	Firm clay	Can be penetrated several inches by thumb with moderate effort	0.05-0.10	7-15
S4	Stiff clay	Readily indented by thumb but penetrated only with great effort	0.10-0.25	15-35
S5	Very stiff clay	Readily indented by thumbnail	0.25-0.50	35-70
S6	Hard clay	Indented with difficulty by thumbnail	>0.50	>70
R0	Extremely weak rock	Indented by thumbnail	0.25-1.0	35-150
R1	Very weak rock	Crumbles under firm blows with point of geological hammer; can be peeled by a pocket knife	1-5	150-725
R2	Weak rock	Can be peeled by a pocket knife with difficulty; shallow indentations made by firm blow with point of geological hammer	5-25	725-3,500
R3	Medium strong rock	Cannot be scraped or peeled with a pocket knife; specimen can be fractured with single firm blow of geological hammer	25-50	3,500-7,000
R4	Strong rock	Specimen requires more than one blow of geological hammer to fracture it	50-100	7,000-15,000
R5	Very strong rock	Specimen requires many blows of geological hammer to fracture it	100-250	15,000-36,000
R6	Extremely strong rock	Specimen can only be chipped with geological hammer	>250	>36,000

Note: Grades S1 to S6 apply to cohesive soils, for example clays, silty clays, and combinations of silts and clays with sand, generally slow draining. Discontinuity wall strength will generally be characterized by grades R0-R6 (rock) while S1-S6 (clay) will generally apply to filled discontinuities.

¹ International Society for Rock Mechanics (ISRM), Commission on standardization of laboratory and field tests (1978): Suggested methods for the quantitative description of discontinuities in rock masses. Int. J. Rock Mech. Min. Sci. & Geomech. Abstr., Vol. 15, No. 6, pp. 319-368.



STATE OF VERMONT
AGENCY OF TRANSPORTATION
CONSTRUCTION AND
MATERIALS BUREAU
CENTRAL LABORATORY

BORING LOG

Jamaica
ER P23-1(216)
Bridge 42, VT Route 30

Boring No.: **B425**
Page No.: 1 of 2
Pin No.: 24b002
Checked By: KAR

Boring Crew: Jeff Nitsch (Seaboard), Lina Maria Pua (WSP)
Date Started: 11/20/24 Date Finished: 11/21/24
VTSPG NAD83: N 235473.24 ft E 1544623.36 ft
Station: 513+98.4 Offset: 0.17 ft R
Ground Elevation: 1213.54 ft

Casing Sampler
Type: WASH BORE SS
I.D.: 4 in 1.5 in
Hammer Wt: 300 lb. 140 lb.
Hammer Fall: N.A. 30 in.
Hammer/Rod Type: Auto
Rig: Mobile B-53 $C_F = 1.55$

Groundwater Observations

Date	Depth (ft)	Notes

Depth (ft)	Strata (1)	CLASSIFICATION OF MATERIALS (Description)	Run (Dip deg.)	Core Rec. % (RQD %)	Drill Rate minutes/ft	Blows/6" (N Value)	Moisture Content %	Gravel %	Sand %	Fines %
		0.0 ft - 0.04 ft, Field Description: A-4, SM, Brown, wet, silty SAND, with roots, [TOPSOIL]				4-10-16-17 (26)	5.6	55.0	29.0	16.0
		0.04 ft - 0.25 ft, Field Description: A-1-a, GP, Black, moist, GRAVEL, with asphalt, [BASE PAVEMENT PREVIOUS BRIDGE]								
		0.25 ft - 2.0 ft, Lab Classification: A-1-b, SM, Brown, moist, medium dense, fine GRAVEL, some fine to coarse sand, little silt, poorly graded, Rec. = 0.96 ft, [FILL]								
5		5.0 ft - 7.0 ft, Lab Classification: A-1-b, SM, Yellowish brown, moist, very dense, fine to coarse GRAVEL, some fine to coarse sand, little fines, poorly graded, Rec. = 1.08 ft, [FILL]				42-41-55-54 (96)	5.7	50.0	32.0	18.0
10		10.0 ft - 12.0 ft, Field Description: A-2-4, SM, Brown, moist, medium dense, fine to medium SAND, little fines, trace angular quartz gravel, poorly graded, Rec. = 0.04 ft, [GLACIOFLUVIAL OUTWASH]				16-12-13-14 (25)				
15		15.0 ft - 17.0 ft, Lab Classification: A-4, ML, Light brown to yellow, wet, hard, SILT, some fine sand, trace fine gravel, laminated structure of fine sand and sandy silt, non-plastic, Rec. = 1.46 ft, [GLACIOFLUVIAL OUTWASH]				18-27-35-42 (62)	17.2	1.0	35.0	64.0
20		20.0 ft - 22.0 ft, Lab Classification: A-4, ML, Light brown to yellow with gray bands, moist, hard, SILT, some fine sand, laminated structure of fine sand and sandy silt, non-plastic, Rec. = 1.5 ft, [GLACIOFLUVIAL OUTWASH]				26-37-44-42 (81)	22.1		35.0	65.0
		23.5 ft - 24.5 ft, Driller noted boulder								
25		25.0 ft - 25.38 ft, Lab Classification: A-4, GM, Light brown to yellow, wet, very dense, silty fine to coarse GRAVEL (partially weathered rock fragments), little fine to coarse sand, poorly graded, Rec. = 0.33 ft, [GLACIAL TILL]				100/4.5" (R)	13.2	44.0	18.0	38.0
		25.38 ft - 28.0 ft, Driller noted cobble zone when washing from 25 to 28 feet bgs.								
		29.5 ft - 30.0 ft, Driller noted increase in roller bit resistance, interpreted								

Notes: 1. Stratification lines represent approximate boundary between material types. Transition may be gradual.
2. N Values have not been corrected for hammer energy. C_F is the hammer energy correction factor.
3. Water level readings have been made at times and under conditions stated. Fluctuations may occur due to other factors than those present at the time measurements were made.



STATE OF VERMONT
AGENCY OF TRANSPORTATION
CONSTRUCTION AND
MATERIALS BUREAU
CENTRAL LABORATORY

BORING LOG

Jamaica
ER P23-1(216)
Bridge 42, VT Route 30

Boring No.: **B425**
Page No.: 2 of 2
Pin No.: 24b002
Checked By: KAR

Boring Crew: Jeff Nitsch (Seaboard), Lina Maria Pua (WSP)
Date Started: 11/20/24 Date Finished: 11/21/24
VTSPG NAD83: N 235473.24 ft E 1544623.36 ft
Station: 513+98.4 Offset: 0.17 ft R
Ground Elevation: 1213.54 ft

Casing Sampler
Type: WASH BORE SS
I.D.: 4 in 1.5 in
Hammer Wt: 300 lb. 140 lb.
Hammer Fall: N.A. 30 in.
Hammer/Rod Type: Auto
Rig: Mobile B-53 $C_F = 1.55$

Groundwater Observations

Date Depth (ft) Notes

Depth (ft)	Strata (1)	CLASSIFICATION OF MATERIALS (Description)	Run (Dip deg.)	Core Rec. % (RQD %)	Drill Rate minutes/ft	Blows/6" (N Value)	Moisture Content %	Gravel %	Sand %	Fines %
35		as partially weathered rock. [WEATHERED ROCK] 30.0 ft - 35.0 ft, Medium gray, fine- to medium-grained, medium strong (R3, bottom 3.9 ft), biotite-quartz GNEISS, completely weathered (W5, top 1.1 ft) to slightly weathered (W2, bottom 3.9 ft); discontinuities shallowly to moderately dipping (up to 45°). closely spaced, tight, irregular, very rough to smooth, with fine to medium sand infilling in some fractures, average 8.0 fractures per foot. Biotite and quartz banding and folding observed throughout run. [MOUNT HOLLY COMPLEX]. NQ. 31.1 ft, No recovery from 30.0 ft bgs to 31.1 ft bgs; interpreted as partially weathered rock washed out during coring.	R1	77 (8)	5.27 3 2.33 4.3 4.25					
40		35.0 ft - 40.0 ft, Brownish gray, fine- to medium-grained, medium strong (R3), biotite-quartz GNEISS, slightly weathered (W2); discontinuities shallowly to moderately dipping, very closely spaced, irregular to planar. smooth to rough, with fine sand infilling in fractures, average 5.2 fractures per foot. Biotite and quartz banding and folding observed throughout run. [MOUNT HOLLY COMPLEX]. NQ. UCS = 6,844 psi.	R2	88 (31)	2.22 3.18 4.73 2.22 3.23					
45		40.0 ft - 45.0 ft, Brown (weathered) to gray, fine- to medium-grained, strong (R4), biotite-quartz GNEISS, slightly weathered (W2); discontinuities shallowly to moderately dipping (up to 45°). very closely to closely spaced, planar to irregular, smooth to rough, with fine sand infilling in fractures, average 5.4 fractures per foot. Biotite and quartz banding observed throughout run. [MOUNT HOLLY COMPLEX]. NQ. UCS = 10,660 psi.	R3	86 (18)	2.43 2.57 2.42 2 2.63					
45		Hole stopped @ 45.0 ft Boring grouted up to 25 ft bgs and then backfilled with drill cuttings to ground surface. Remarks: 1. The as-drilled boring locations and elevations are derived from electronic file "x24b002sv.dgn" provided to WSP by VTrans on December 18, 2024. 2. AASHTO and USCS classifications are based on visual description of sample recovery at depths where laboratory testing not performed. 3. The SPT sample at 0-2 ft bgs was obtained 2.2 feet north of the as-drilled B425 location due to a damaged spoon sampler. No casing was inserted at this offset location.								
50										
55										

Notes: 1. Stratification lines represent approximate boundary between material types. Transition may be gradual.
2. N Values have not been corrected for hammer energy. C_F is the hammer energy correction factor.
3. Water level readings have been made at times and under conditions stated. Fluctuations may occur due to other factors than those present at the time measurements were made.



STATE OF VERMONT
AGENCY OF TRANSPORTATION
CONSTRUCTION AND
MATERIALS BUREAU
CENTRAL LABORATORY

BORING LOG

Jamaica
ER P23-1(216)
Bridge 42, VT Route 30

Boring No.: **B545**
Page No.: 1 of 2
Pin No.: 24b002
Checked By: KAR

Boring Crew: Jeff Nitsch (Seaboard), Lina Maria Pua (WSP)
Date Started: 11/19/24 Date Finished: 11/20/24
VTSPG NAD83: N 235482.99 ft E 1544453.26 ft
Station: 515+68.6 Offset: 7.39 ft L
Ground Elevation: 1220.37 ft

Casing Sampler
Type: WASH BORE SS
I.D.: 4 in 1.5 in
Hammer Wt: 300 lb. 140 lb.
Hammer Fall: N.A. 30 in.
Hammer/Rod Type: Auto
Rig: Mobile B-53 $C_F = 1.55$

Groundwater Observations

Date	Depth (ft)	Notes
11/20/24	13.5	9:20 AM after core

Depth (ft)	Strata (1)	CLASSIFICATION OF MATERIALS (Description)	Run (Dip deg.)	Core Rec. % (RQD %)	Drill Rate minutes/ft	Blows/6" (N Value)	Moisture Content %	Gravel %	Sand %	Fines %
0		0.0 ft - 0.08 ft, Field Description: A-2-4, SM, Brown, fine SAND, some silt, roots and grass, [TOPSOIL]				37-19-25-15 (44)	2.1	74.0	22.1	3.9
0.08		0.08 ft - 0.58 ft, Lab Classification: A-1-a, SW, Black, dry, dense, fine to coarse GRAVEL, some coarse to medium sand with asphalt, trace fines, well graded, [BASE PAVEMENT PREVIOUS BRIDGE]					2.6	47.0	42.0	11.0
0.58		0.58 ft - 2.0 ft, Lab Classification: A-1-b, SP-SM, Light brown to yellow, dry, dense, sandy fine rounded to subrounded GRAVEL, little fines, poorly graded, Rec. = 1.5 ft, [FILL]								
5		5.0 ft - 7.0 ft, Lab Classification: A-1-a, SM, Light brown to yellow, moist, dense, fine to coarse rounded to angular GRAVEL, some fine to coarse sand, little fines, poorly graded, Rec. = 0.58 ft, [GLACIOFLUVIAL OUTWASH]				17-28-22-13 (50)	9.2	55.0	32.0	13.0
10		10.0 ft - 12.0 ft, Lab Classification: A-4, ML, Light brown to yellow, moist, hard, sandy SILT, trace fine gravel, lenses of fine sand, non-plastic, Rec. = 1.33 ft, [GLACIOFLUVIAL OUTWASH]				21-26-31-34 (57)	17.8	3.0	46.0	51.0
15		15.0 ft - 15.83 ft, Lab Classification: A-4, SM, Light brown to yellow, moist, very dense, silty SAND, little fine gravel, poorly graded, Rec. = 0.54 ft, [GLACIOFLUVIAL OUTWASH]				50-50/4" (R)	13.7	17.0	45.0	38.0
20		20.0 ft - 20.17 ft, Field Description: A-2-4, SM, Light brown, moist, very dense, fine to medium SAND, some fines, trace gravel, Rec. = 0.1 ft, [GLACIOFLUVIAL OUTWASH] 20.17 ft - 20.42 ft, Sampled with 3" OD split spoon; no recovery, Rec. = 0.0 ft 20.42 ft, Gravel and cobbles observed in wash water.				50/2" (R) (R)				
25		25.0 ft - 25.33 ft, Lab Classification: A-4, SM, Light brown to yellow, moist, very dense, silty fine to coarse SAND, little fine gravel, little mica, poorly graded, Rec. = 0.04 ft, [GLACIAL TILL] 25.33 ft - 25.54 ft, Sampled with 3" OD split spoon; no recovery, Rec. = 0.0 ft 25.54 ft, Gravel and cobbles observed in wash water.				100/4" (R) (R)	13.1	13.0	50.0	37.0

Notes:

1. Stratification lines represent approximate boundary between material types. Transition may be gradual.
2. N Values have not been corrected for hammer energy. C_F is the hammer energy correction factor.
3. Water level readings have been made at times and under conditions stated. Fluctuations may occur due to other factors than those present at the time measurements were made.

APPENDIX B

Rock Core Photographs

Appendix B
Rock Core Photographs
Bridge 42, VT Route 30
VTrans Jamaica ER P23-1(216)
Jamaica, Vermont

Boring	Run	Depth Below Surface			Recovery			RQD			Rock Type	Box Row	Date Cored		
		Feet			Feet		%	Feet		%					
B425	R1	30.0	-	35.0	3.9	/	5.0	77	0.4	/	5.0	8	GNEISS	Row 1	11/21/2024
	R2	35.0	-	40.0	4.4	/	5.0	88	1.6	/	5.0	31	GNEISS	Row 2	11/21/2024
	R3	40.0	-	45.0	4.3	/	5.0	86	0.9	/	5.0	18	GNEISS	Row 3	11/21/2024



Notes:

1. "Box row" indicates the section of the box where the core is contained: 1 = top, 4 = bottom.
2. Top of each core run is on the left and increases with depth to the right.

Prepared By: LMP
 Checked By: KAR
 Reviewed By: JDL

Appendix B
Rock Core Photographs
Bridge 42, VT Route 30
VTrans Jamaica ER P23-1(216)
Jamaica, Vermont

Boring	Run	Depth Below Surface		Recovery			RQD		Rock Type	Box Row	Date Cored
		Feet		Feet		%	Feet	%			
B545	R1	35.2	- 40.2	4.7	/ 5.0	93	2.8 / 5.0	56	GNEISS	Row 1	11/20/2024
	R2	40.2	- 45.2	5.0	/ 5.0	100	2.6 / 5.0	52	GNEISS	Row 2	11/20/2024



Notes:

1. "Box row" indicates the section of the box where the core is contained: 1 = top, 4 = bottom.
2. Top of each core run is on the left and increases with depth to the right.

Prepared By: LMP
 Checked By: KAR
 Reviewed By: JDL

APPENDIX C

Laboratory Test Results

Client:	WSP USA, Inc.		
Project:	VTrans Jamaica Bridge 42		
Location:	Jamaica, VT	Project No:	GTX-320233
Boring ID: ---	Sample Type: ---	Tested By:	ajl
Sample ID: ---	Test Date: 12/10/24	Checked By:	ank
Depth : ---	Test Id: 795235		

Moisture Content of Soil and Rock - ASTM D2216

Boring ID	Sample ID	Depth	Description	Moisture Content, %
B425	S1B	0.25-0.96'	Moist, grayish brown silty sand with gravel	5.6
B425	S2	5-7'	Moist, yellowish brown silty sand with gravel	5.7
B425	S4	15-17'	Moist, brown sandy silt	17.2
B425	S5	20-22'	Moist, grayish brown sandy silt	22.1
B425	S6	25-27'	Moist, grayish brown silty gravel with sand	13.2
B545	S1A	0.08-0.58'	Moist, dark yellowish brown sand with gravel	2.1
B545	S1B	0.58-1.5'	Moist, yellowish brown sand with silt and gravel	2.6

Notes: Temperature of Drying : 110° Celsius



Client:	WSP USA, Inc.		
Project:	VTrans Jamaica Bridge 42		
Location:	Jamaica, VT	Project No:	GTX-320233
Boring ID:	---	Sample Type:	---
Sample ID:	---	Test Date:	12/10/24
Depth :	---	Test Id:	795238
		Tested By:	ajl
		Checked By:	ank

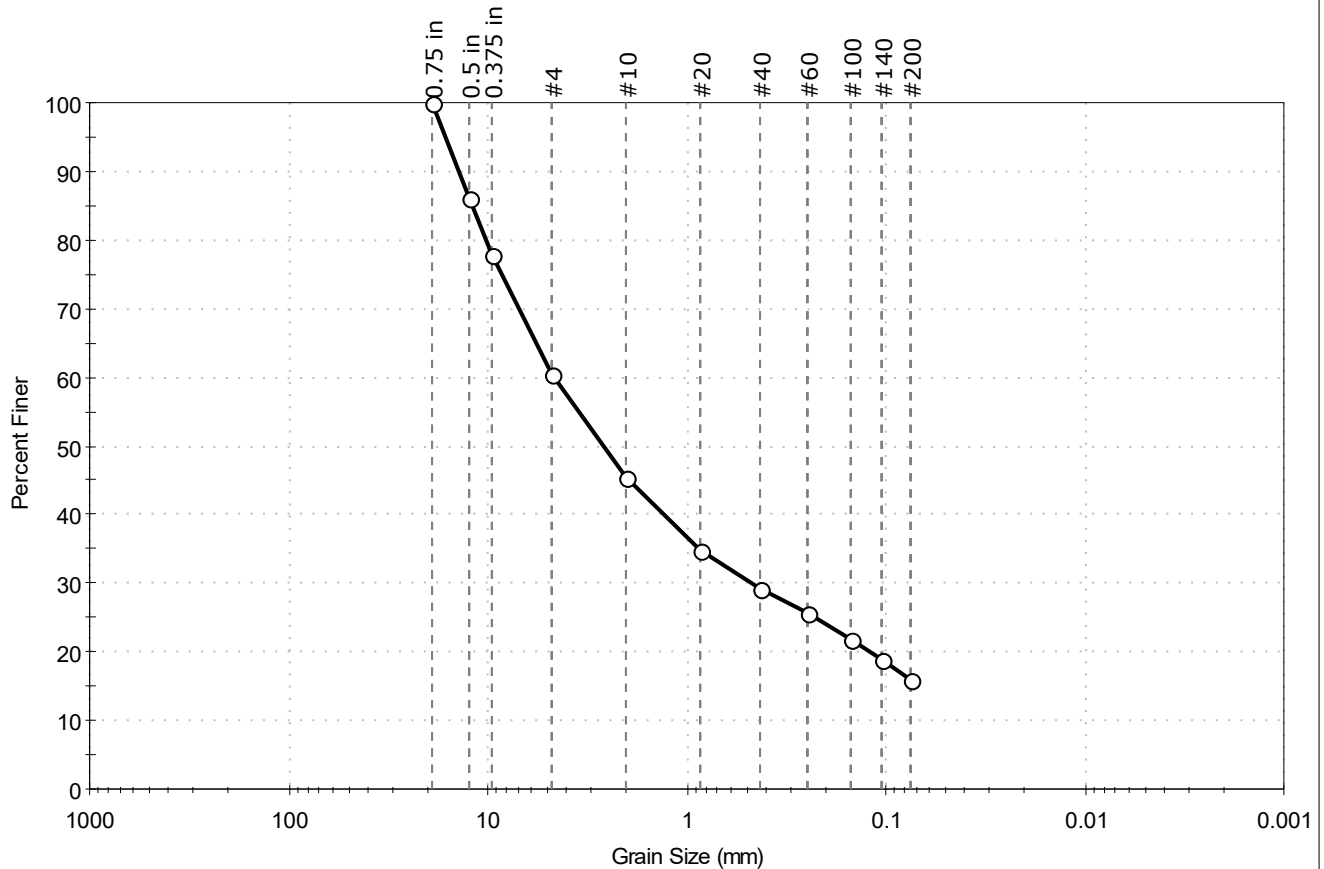
Moisture Content of Soil and Rock - ASTM D2216

Boring ID	Sample ID	Depth	Description	Moisture Content, %
B545	S2	5-7'	Moist, grayish brown silty sand with gravel	9.2
B545	S3	10-12'	Moist, yellowish brown sandy silt	17.8
B545	S4	15-15.83'	Moist, yellowish brown silty sand	13.7
B545	S7	25-25.33'	Moist, yellowish brown silty sand	13.1

Notes: Temperature of Drying : 110° Celsius

Client: WSP USA, Inc.	Project No: GTX-320233	
Project: VTrans Jamaica Bridge 42		
Location: Jamaica, VT		
Boring ID: B425	Sample Type: Jar	Tested By: ajl
Sample ID: S1B	Test Date: 12/12/24	Checked By: ank
Depth : 0.25-0.96'	Test Id: 795219	
Test Comment: ---		
Visual Description: Moist, grayish brown silty sand with gravel		
Sample Comment: ---		

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	39.4	44.8	15.8

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.75 in	19.00	100		
0.5 in	12.50	86		
0.375 in	9.50	78		
#4	4.75	61		
#10	2.00	45		
#20	0.85	35		
#40	0.425	29		
#60	0.25	26		
#100	0.15	22		
#140	0.11	19		
#200	0.075	16		

Coefficients

D₈₅ = 12.0510 mm D₃₀ = 0.4618 mm
 D₆₀ = 4.5923 mm D₁₅ = N/A
 D₅₀ = 2.5981 mm D₁₀ = N/A
 C_u = N/A C_c = N/A

Classification

ASTM N/A

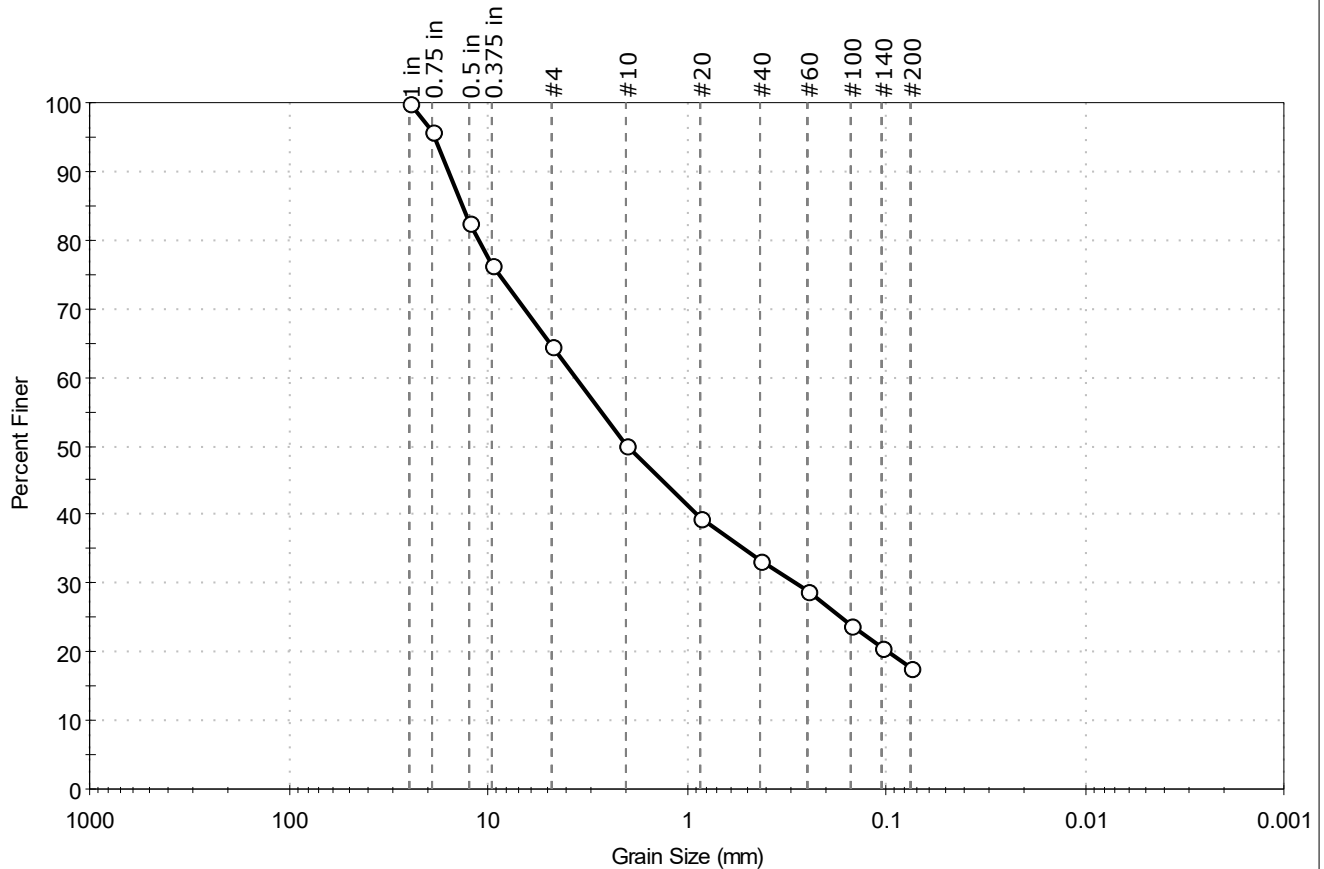
AASHTO Stone Fragments, Gravel and Sand (A-1-b (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client: WSP USA, Inc.	Project No: GTX-320233
Project: VTrans Jamaica Bridge 42	
Location: Jamaica, VT	
Boring ID: B425	Sample Type: Jar
Sample ID: S2	Test Date: 12/12/24
Depth: 5-7'	Test Id: 795220
Test Comment: ---	Tested By: ajl
Visual Description: Moist, yellowish brown silty sand with gravel	Checked By: ank
Sample Comment: ---	

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	35.3	46.9	17.8

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 in	25.00	100		
0.75 in	19.00	96		
0.5 in	12.50	83		
0.375 in	9.50	76		
#4	4.75	65		
#10	2.00	50		
#20	0.85	39		
#40	0.42	33		
#60	0.25	29		
#100	0.15	24		
#140	0.11	21		
#200	0.075	18		

Coefficients

D₈₅ = 13.4753 mm D₃₀ = 0.2889 mm
 D₆₀ = 3.6145 mm D₁₅ = N/A
 D₅₀ = 1.9986 mm D₁₀ = N/A
 C_u = N/A C_c = N/A

Classification

ASTM N/A

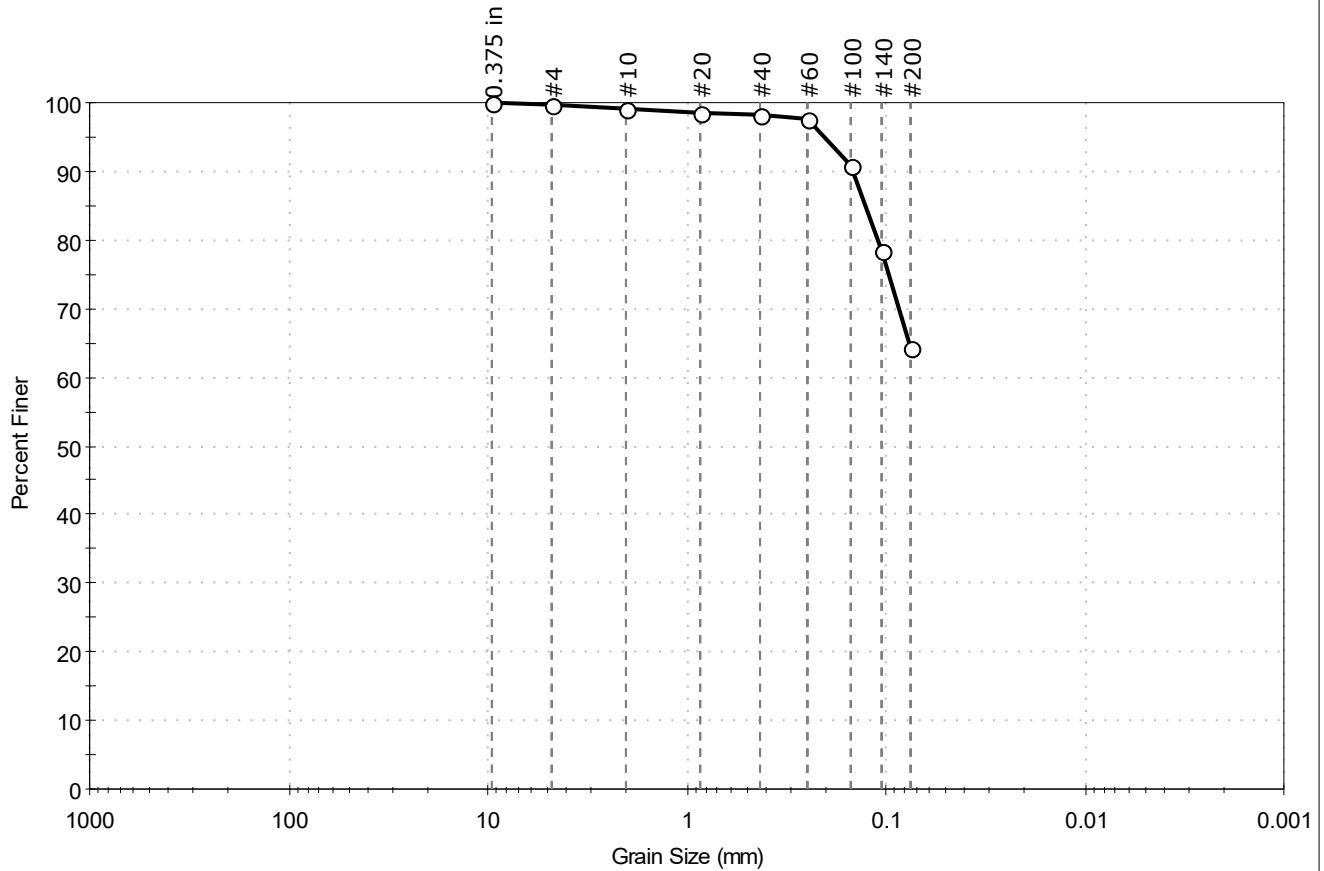
AASHTO Stone Fragments, Gravel and Sand (A-1-b (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client: WSP USA, Inc.	Project No: GTX-320233
Project: VTrans Jamaica Bridge 42	
Location: Jamaica, VT	
Boring ID: B425	Sample Type: Jar
Sample ID: S4	Test Date: 12/12/24
Depth: 15-17'	Test Id: 795221
Test Comment: ---	Tested By: ajl
Visual Description: Moist, brown sandy silt	Checked By: ank
Sample Comment: ---	

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	0.2	35.4	64.4

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.375 in	9.50	100		
#4	4.75	100		
#10	2.00	99		
#20	0.85	99		
#40	0.42	98		
#60	0.25	98		
#100	0.15	91		
#140	0.11	78		
#200	0.075	64		

Coefficients

$D_{85} = 0.1274$ mm $D_{30} = \text{N/A}$
 $D_{60} = \text{N/A}$ $D_{15} = \text{N/A}$
 $D_{50} = \text{N/A}$ $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

AASHTO Silty Soils (A-4 (0))

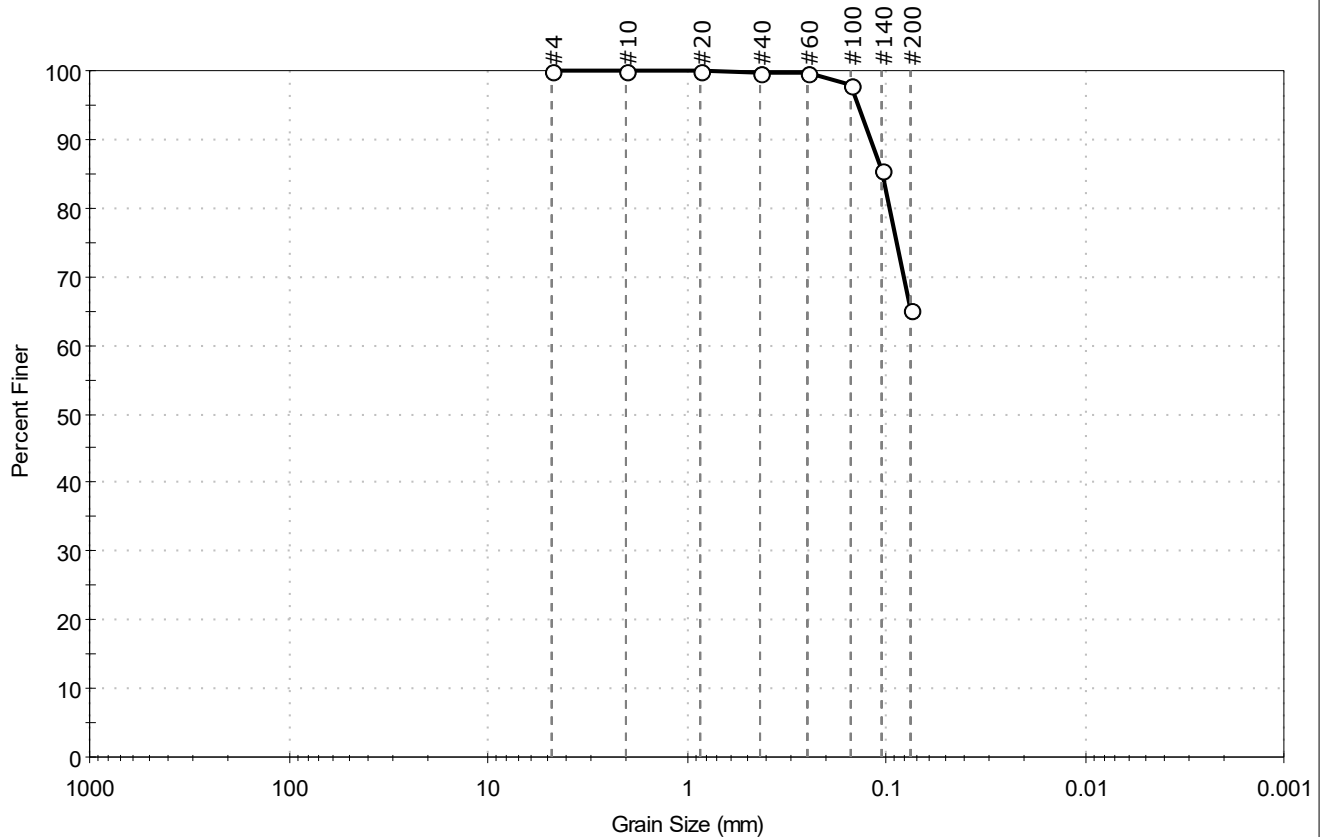
Sample/Test Description

Sand/Gravel Particle Shape : ---

Sand/Gravel Hardness : ---

Client: WSP USA, Inc.	Project No: GTX-320233	
Project: VTrans Jamaica Bridge 42		
Location: Jamaica, VT		
Boring ID: B425	Sample Type: Jar	Tested By: ajl
Sample ID: S5	Test Date: 12/12/24	Checked By: ank
Depth : 20-22'	Test Id: 795222	
Test Comment: ---		
Visual Description: Moist, grayish brown sandy silt		
Sample Comment: ---		

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	0.0	34.8	65.2

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
#4	4.75	100		
#10	2.00	100		
#20	0.85	100		
#40	0.42	100		
#60	0.25	100		
#100	0.15	98		
#140	0.11	86		
#200	0.075	65		

Coefficients

$D_{85} = 0.1049$ mm $D_{30} = \text{N/A}$
 $D_{60} = \text{N/A}$ $D_{15} = \text{N/A}$
 $D_{50} = \text{N/A}$ $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

AASHTO Silty Soils (A-4 (0))

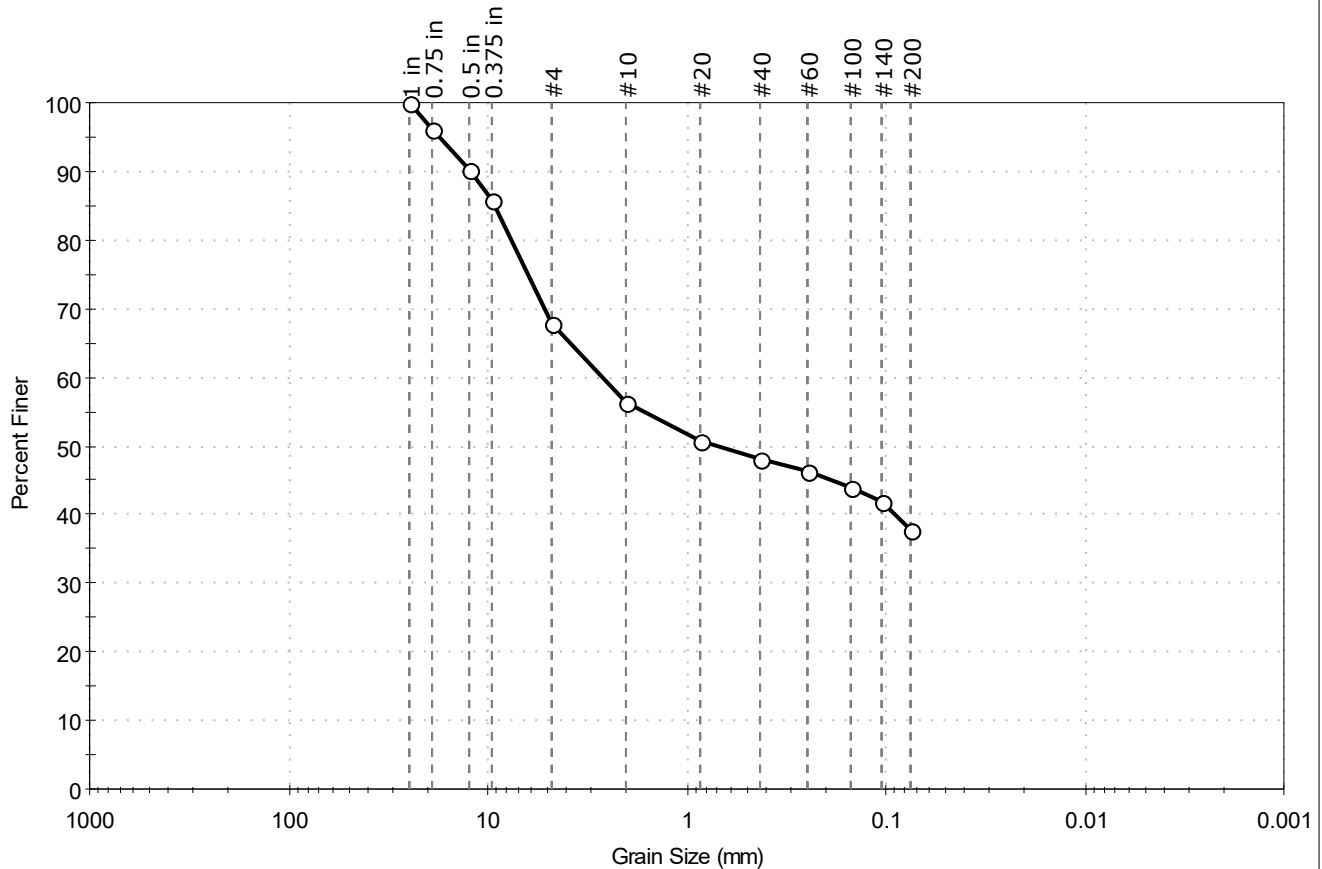
Sample/Test Description

Sand/Gravel Particle Shape : ---

Sand/Gravel Hardness : ---

Client:	WSP USA, Inc.	Project No:	GTX-320233
Project:	VTrans Jamaica Bridge 42		
Location:	Jamaica, VT		
Boring ID:	B425	Sample Type:	Jar
Sample ID:	S6	Test Date:	12/12/24
Depth :	25-27'	Test Id:	795223
Test Comment:	---		
Visual Description:	Moist, grayish brown silty gravel with sand		
Sample Comment:	---		

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	32.1	30.2	37.7

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1 in	25.00	100		
0.75 in	19.00	96		
0.5 in	12.50	90		
0.375 in	9.50	86		
#4	4.75	68		
#10	2.00	56		
#20	0.85	51		
#40	0.42	48		
#60	0.25	46		
#100	0.15	44		
#140	0.11	42		
#200	0.075	38		

Coefficients

D ₈₅ = 9.2018 mm	D ₃₀ = N/A
D ₆₀ = 2.6327 mm	D ₁₅ = N/A
D ₅₀ = 0.7110 mm	D ₁₀ = N/A
C _u = N/A	C _c = N/A

Classification

ASTM N/A

AASHTO Silty Soils (A-4 (0))

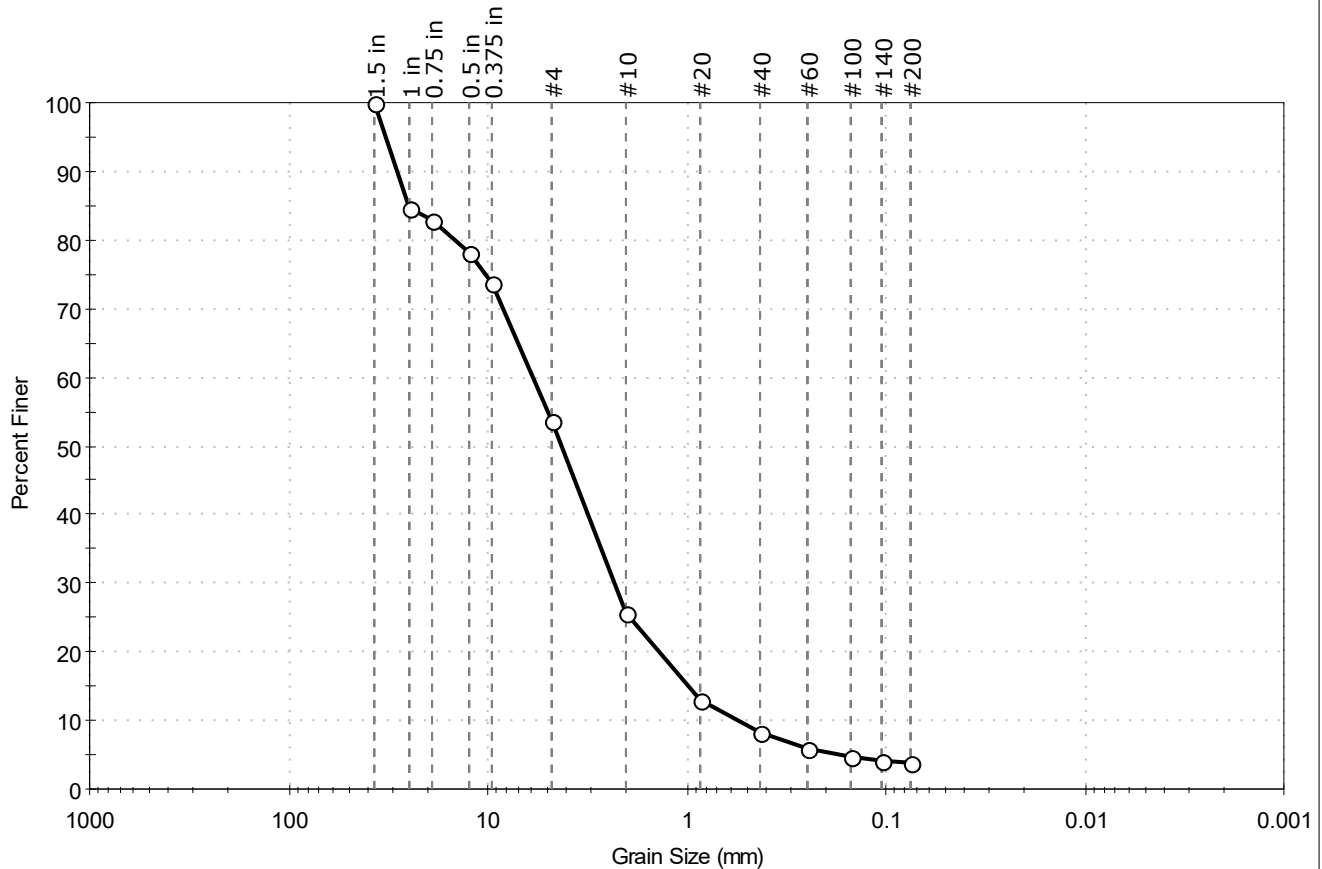
Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR

Sand/Gravel Hardness : HARD

Client: WSP USA, Inc.	Project No: GTX-320233
Project: VTrans Jamaica Bridge 42	
Location: Jamaica, VT	
Boring ID: B545	Sample Type: Jar
Sample ID: S1A	Test Date: 12/12/24
Depth: 0.08-0.58'	Test Id: 795224
Test Comment: ---	
Visual Description: Moist, dark yellowish brown sand with gravel	
Sample Comment: ---	

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	46.3	49.8	3.9

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1.5 in	37.50	100		
1 in	25.00	85		
0.75 in	19.00	83		
0.5 in	12.50	78		
0.375 in	9.50	74		
#4	4.75	54		
#10	2.00	26		
#20	0.85	13		
#40	0.42	8		
#60	0.25	6		
#100	0.15	5		
#140	0.11	4		
#200	0.075	3.9		

Coefficients

$D_{85} = 25.2238$ mm $D_{30} = 2.2803$ mm
 $D_{60} = 5.8993$ mm $D_{15} = 0.9658$ mm
 $D_{50} = 4.2361$ mm $D_{10} = 0.5492$ mm
 $C_u = 10.742$ $C_c = 1.605$

Classification

ASTM Well-graded SAND with Gravel (SW)

AASHTO Stone Fragments, Gravel and Sand (A-1-a (1))

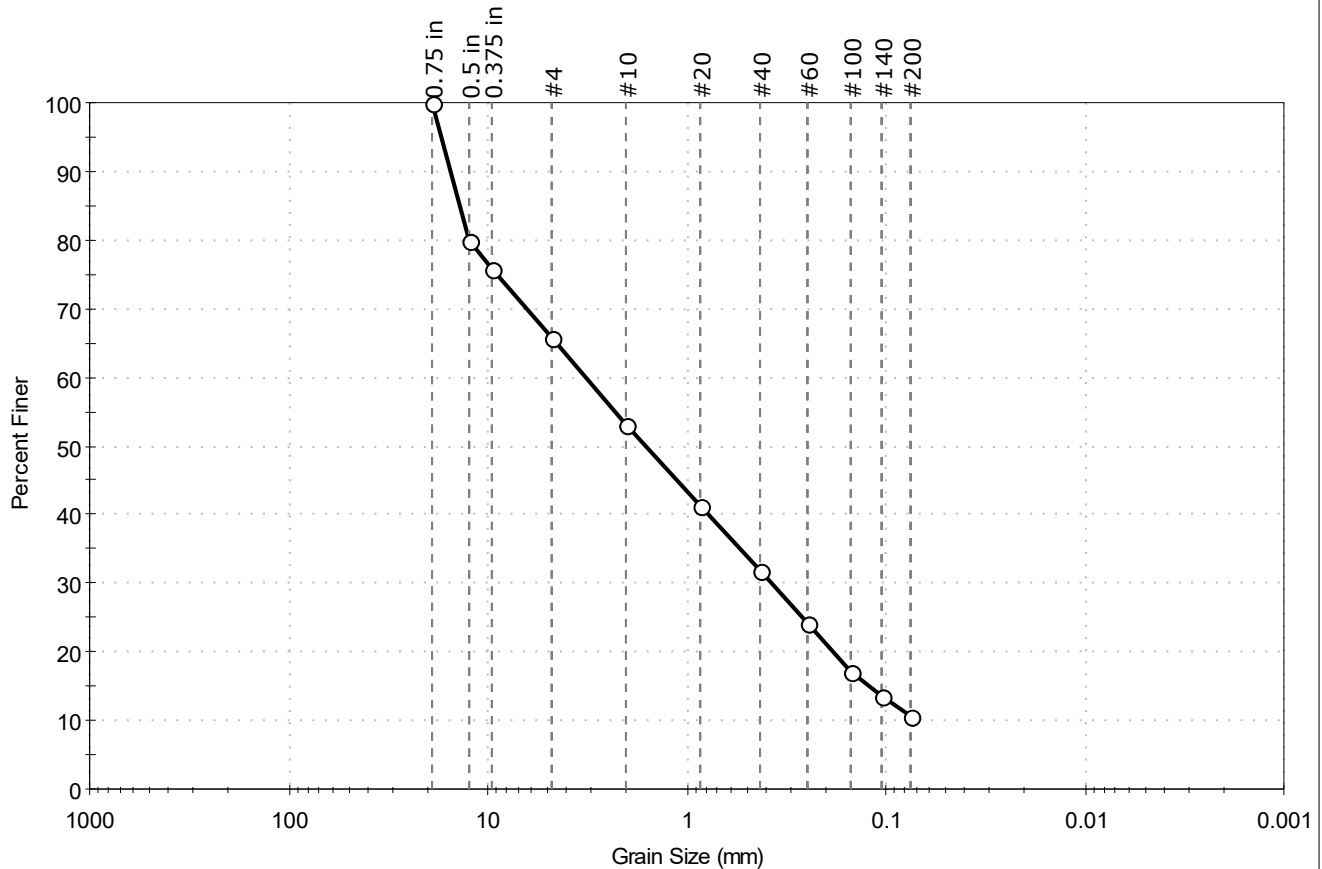
Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR

Sand/Gravel Hardness : HARD

Client: WSP USA, Inc.	Project No: GTX-320233
Project: VTrans Jamaica Bridge 42	
Location: Jamaica, VT	
Boring ID: B545	Sample Type: Jar
Sample ID: S1B	Test Date: 12/12/24
Depth: 0.58-1.5'	Test Id: 795225
Test Comment: ---	
Visual Description: Moist, yellowish brown sand with silt and gravel	
Sample Comment: ---	

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	34.3	55.0	10.7

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.75 in	19.00	100		
0.5 in	12.50	80		
0.375 in	9.50	76		
#4	4.75	66		
#10	2.00	53		
#20	0.85	41		
#40	0.42	32		
#60	0.25	24		
#100	0.15	17		
#140	0.11	14		
#200	0.075	11		

Coefficients

$D_{85} = 13.8865 \text{ mm}$ $D_{30} = 0.3761 \text{ mm}$
 $D_{60} = 3.2002 \text{ mm}$ $D_{15} = 0.1210 \text{ mm}$
 $D_{50} = 1.5900 \text{ mm}$ $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

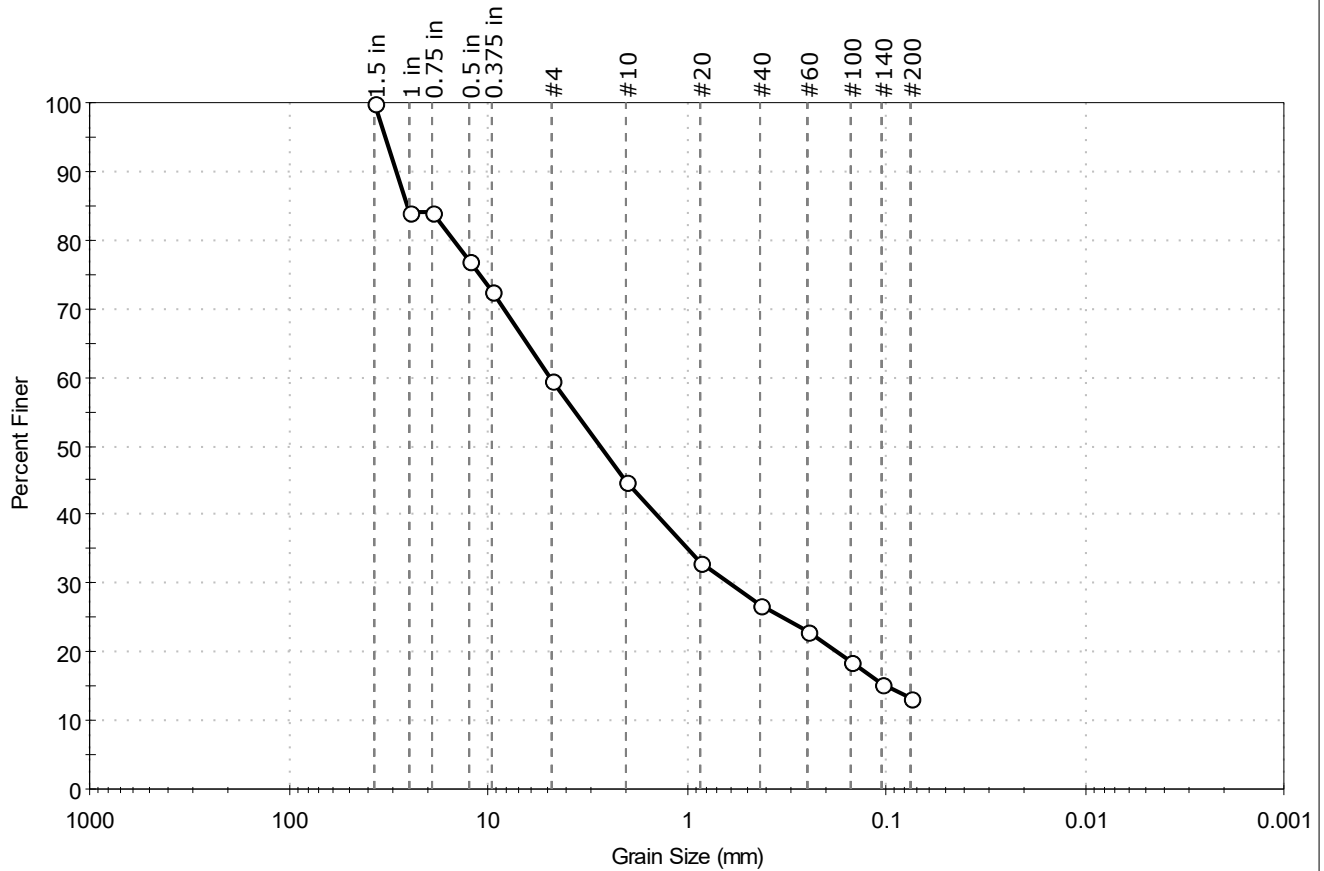
AASHTO Stone Fragments, Gravel and Sand (A-1-b (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client: WSP USA, Inc.	Project No: GTX-320233
Project: VTrans Jamaica Bridge 42	
Location: Jamaica, VT	
Boring ID: B545	Sample Type: Jar
Sample ID: S2	Tested By: ajl
Depth: 5-7'	Test Date: 12/12/24
	Checked By: ank
	Test Id: 795226
Test Comment: ---	
Visual Description: Moist, grayish brown silty sand with gravel	
Sample Comment: ---	

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	40.3	46.4	13.3

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
1.5 in	37.50	100		
1 in	25.00	84		
0.75 in	19.00	84		
0.5 in	12.50	77		
0.375 in	9.50	73		
#4	4.75	60		
#10	2.00	45		
#20	0.85	33		
#40	0.42	27		
#60	0.25	23		
#100	0.15	19		
#140	0.11	15		
#200	0.075	13		

Coefficients

$D_{85} = 25.6381$ mm $D_{30} = 0.6092$ mm
 $D_{60} = 4.8311$ mm $D_{15} = 0.0984$ mm
 $D_{50} = 2.6979$ mm $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

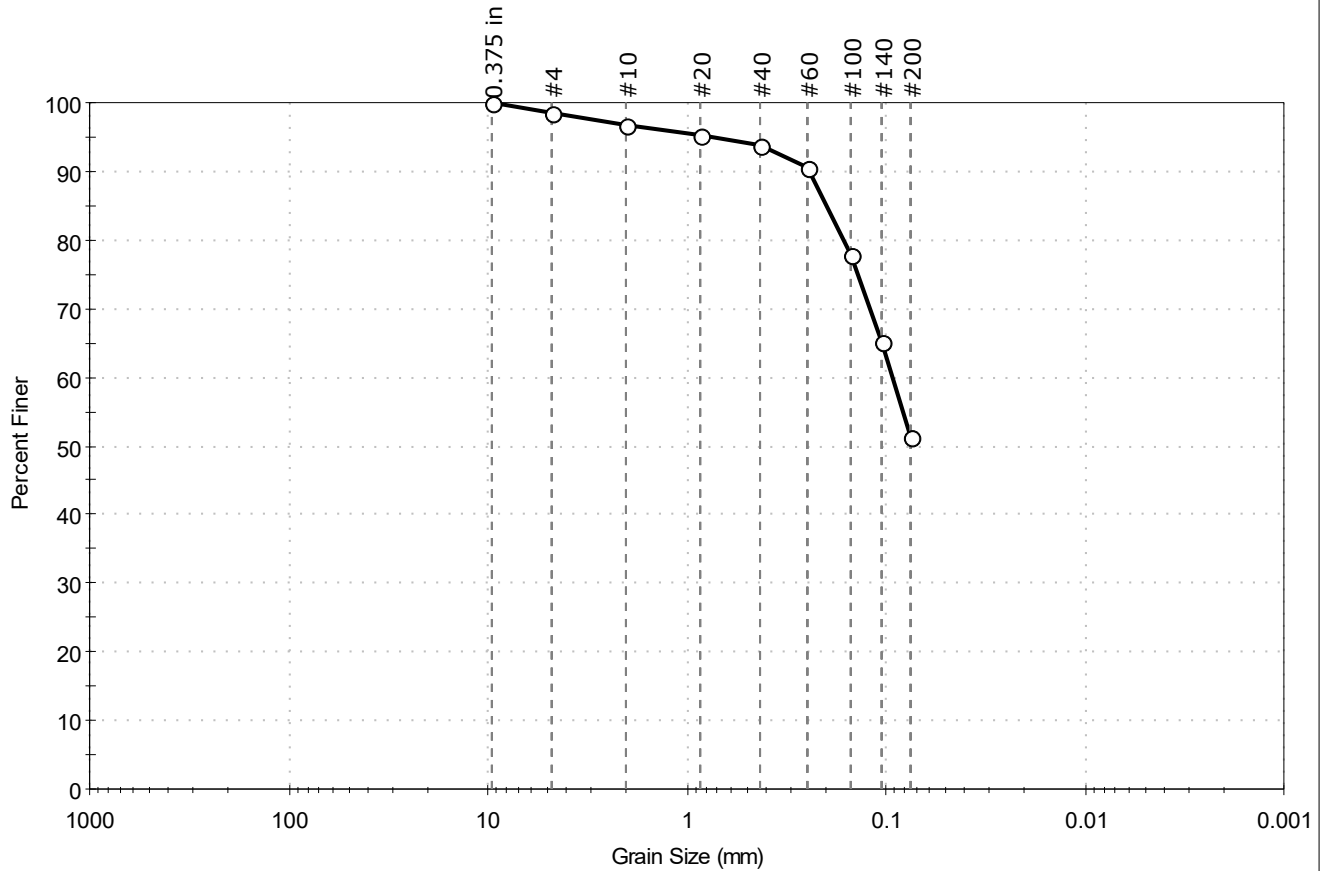
AASHTO Stone Fragments, Gravel and Sand (A-1-a (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client: WSP USA, Inc.	Project No: GTX-320233	
Project: VTrans Jamaica Bridge 42		
Location: Jamaica, VT		
Boring ID: B545	Sample Type: Jar	Tested By: ajl
Sample ID: S3	Test Date: 12/12/24	Checked By: ank
Depth: 10-12'	Test Id: 795520	
Test Comment: ---		
Visual Description: Moist, yellowish brown sandy silt		
Sample Comment: ---		

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	1.6	47.2	51.2

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.375 in	9.50	100		
#4	4.75	98		
#10	2.00	97		
#20	0.85	95		
#40	0.42	94		
#60	0.25	90		
#100	0.15	78		
#140	0.11	65		
#200	0.075	51		

Coefficients

$D_{85} = 0.2010 \text{ mm}$ $D_{30} = \text{N/A}$
 $D_{60} = 0.0934 \text{ mm}$ $D_{15} = \text{N/A}$
 $D_{50} = \text{N/A}$ $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

AASHTO Silty Soils (A-4 (0))

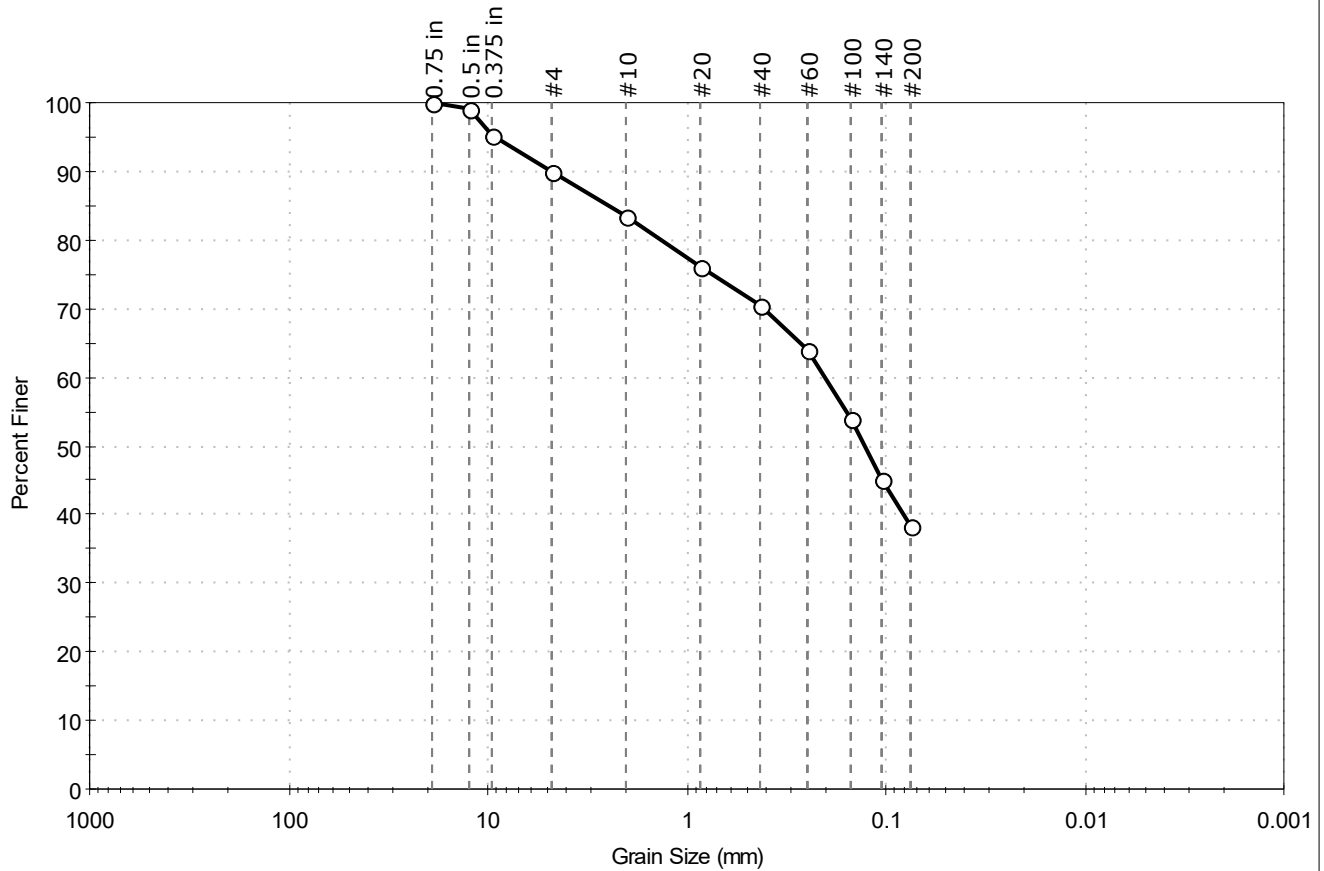
Sample/Test Description

Sand/Gravel Particle Shape : ---

Sand/Gravel Hardness : ---

Client: WSP USA, Inc.	Project No: GTX-320233
Project: VTrans Jamaica Bridge 42	
Location: Jamaica, VT	
Boring ID: B545	Sample Type: Jar
Sample ID: S4	Test Date: 12/12/24
Depth: 15-15.83'	Test Id: 795227
Test Comment: ---	
Visual Description: Moist, yellowish brown silty sand	
Sample Comment: ---	

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	10.2	51.4	38.4

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.75 in	19.00	100		
0.5 in	12.50	99		
0.375 in	9.50	95		
#4	4.75	90		
#10	2.00	83		
#20	0.85	76		
#40	0.42	70		
#60	0.25	64		
#100	0.15	54		
#140	0.11	45		
#200	0.075	38		

Coefficients

$D_{85} = 2.4923 \text{ mm}$ $D_{30} = \text{N/A}$
 $D_{60} = 0.2042 \text{ mm}$ $D_{15} = \text{N/A}$
 $D_{50} = 0.1288 \text{ mm}$ $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

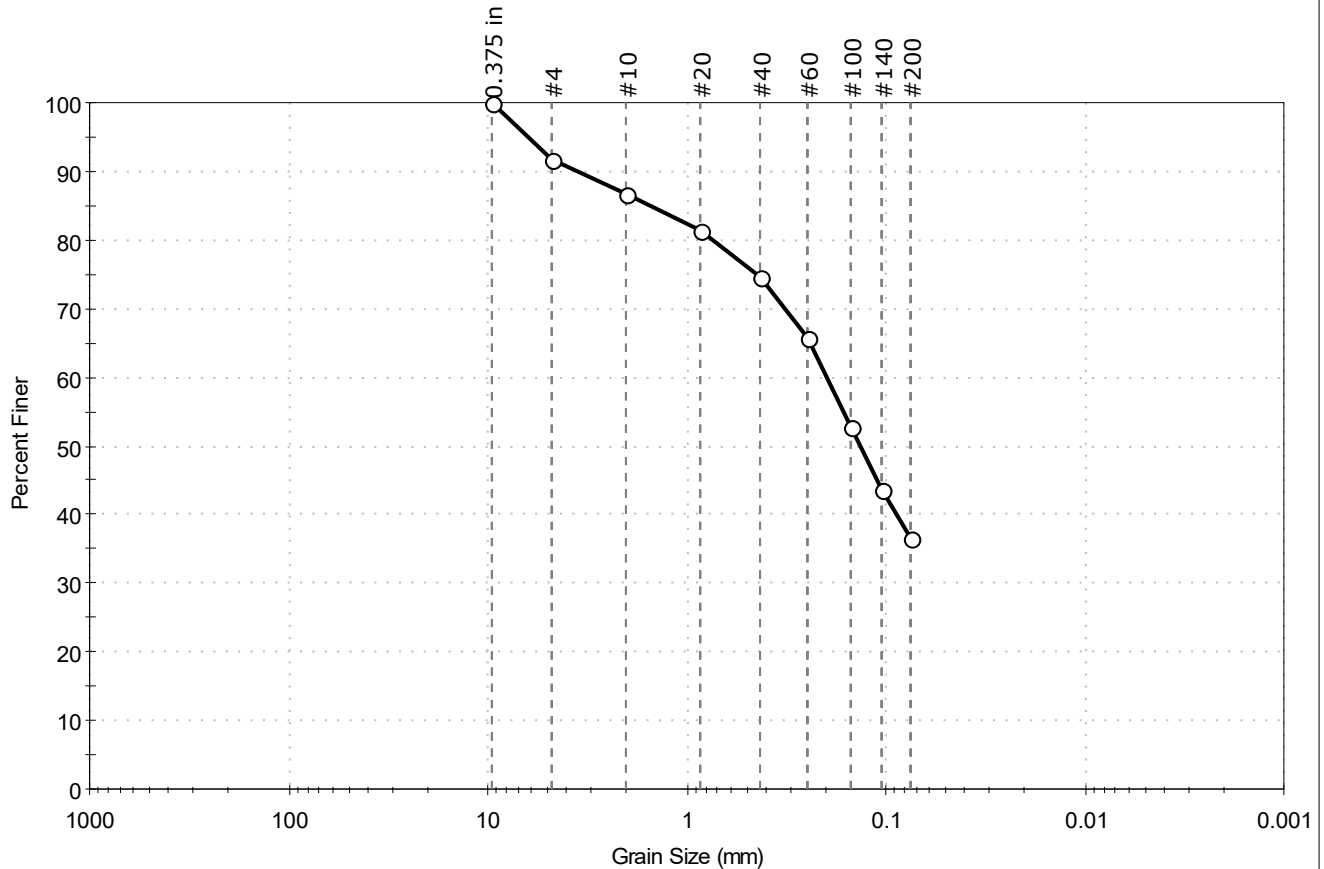
AASHTO Silty Soils (A-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client: WSP USA, Inc.	Project No: GTX-320233
Project: VTrans Jamaica Bridge 42	
Location: Jamaica, VT	
Boring ID: B545	Sample Type: Jar
Sample ID: S7	Test Date: 12/12/24
Depth: 25-25.33'	Test Id: 795228
Test Comment: ---	Tested By: ajl
Visual Description: Moist, yellowish brown silty sand	Checked By: ank
Sample Comment: ---	

Particle Size Analysis - ASTM D6913



% Cobble	% Gravel	% Sand	% Silt & Clay Size
—	8.2	55.1	36.7

Sieve Name	Sieve Size, mm	Percent Finer	Spec. Percent	Complies
0.375 in	9.50	100		
#4	4.75	92		
#10	2.00	87		
#20	0.85	81		
#40	0.42	75		
#60	0.25	66		
#100	0.15	53		
#140	0.11	44		
#200	0.075	37		

Coefficients

$D_{85} = 1.5151 \text{ mm}$ $D_{30} = \text{N/A}$
 $D_{60} = 0.1989 \text{ mm}$ $D_{15} = \text{N/A}$
 $D_{50} = 0.1341 \text{ mm}$ $D_{10} = \text{N/A}$
 $C_u = \text{N/A}$ $C_c = \text{N/A}$

Classification

ASTM N/A

AASHTO Silty Soils (A-4 (0))

Sample/Test Description

Sand/Gravel Particle Shape : ANGULAR
 Sand/Gravel Hardness : HARD

Client:	WSP USA, Inc.	Project No:	GTX-320233
Project:	VTrans Jamaica Bridge 42		
Location:	Jamaica, VT		
Boring ID:	---	Sample Type:	---
Sample ID:	---	Test Date:	12/11/24
Depth :	---	Test Id:	795218
		Tested By:	gp
		Checked By:	smd

Bulk Density and Compressive Strength of Rock Core Specimens by ASTM D7012 Method C

Boring ID	Sample Number	Depth	Bulk Density, pcf	Compressive strength, psi	Failure Type	Meets ASTM D4543	Note(s)
B425	Run 2	36.7-37.05 ft	168	6844	1	No	1,*
B425	Run 3	43.6-44.0 ft	169	10660	1	No	1 , 2,*
B545	Run 1	38.54-38.91 ft	166	15924	1	No	1 , 2,*
B545	Run 2	44.23-44.61 ft	167	20093	1	No	1 , 2,*

- Notes: Density determined on core samples by measuring dimensions and weight and then calculating.
- All specimens tested at the approximate as-received moisture content and at standard laboratory temperature.
- The axial load was applied continuously at a stress rate that produced failure in a test time between 2 and 15 minutes.
- Failure Type: 1 = Intact Material Failure; 2 = Discontinuity Failure; 3 = Intact Material and Discontinuity Failure (See attached photographs)
- 1: Best effort end preparation. See Tolerance report for details.
 - 2: The as-received core did not meet the ASTM side straightness tolerance due to irregularities in the sample as cored.
 - 3: Specimen L/D < 2.
 - 4: The as-received core did not meet the ASTM minimum diameter tolerance of 1.875 inches.
 - 5: Specimen diameter is less than 10 times maximum particle size.
 - 6: Specimen diameter is less than 6 times maximum particle size.

*Because the indicated tested specimens did not meet the ASTM D4543 standard tolerances, the results reported here may differ from those for a test specimen within tolerances.

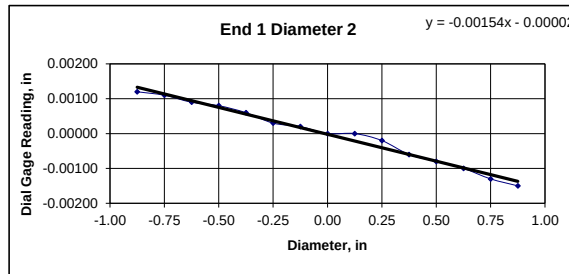
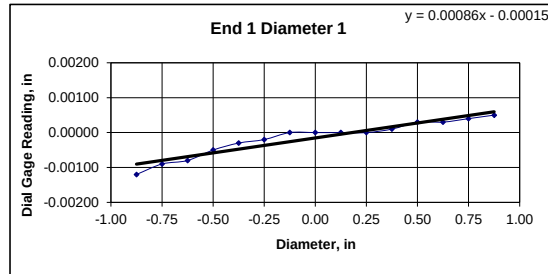


Client:	WSP USA, Inc.	Test Date:	12/10/2024
Project Name:	Vtrans Jamaica Bridge 42	Tested By:	jss
Project Location:	Jamaica, VT	Checked By:	smd
GTx #:	320233		
Boring ID:	B425		
Sample ID:	Run 2		
Depth, ft:	36.7-37.05		
Visual Description:	See photographs		

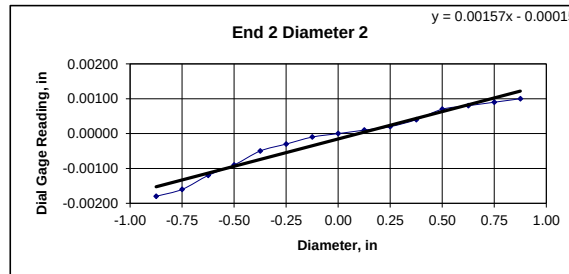
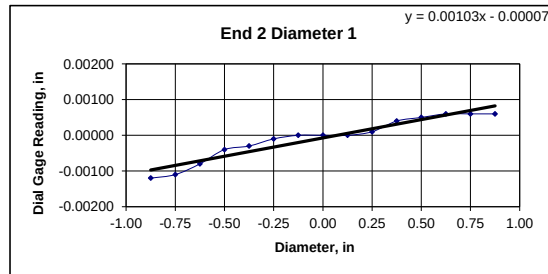
UNIT WEIGHT DETERMINATION AND DIMENSIONAL AND SHAPE TOLERANCES OF ROCK CORE SPECIMENS BY ASTM D4543

BULK DENSITY				DEVIATION FROM STRAIGHTNESS (Procedure S1)	
	1	2	Average	Maximum gap between side of core and reference surface plate: Is the maximum gap ≤ 0.02 in.? YES	
Specimen Length, in:	4.19	4.19	4.19	Maximum difference must be < 0.020 in. Straightness Tolerance Met? YES	
Specimen Diameter, in:	1.99	1.99	1.99		
Specimen Mass, g:	575.31				
Bulk Density, lb/ft ³	168				
Length to Diameter Ratio:	2.1	Minimum Diameter Tolerance Met? YES	Length to Diameter Ratio Tolerance Met? YES		

END FLATNESS AND PARALLELISM (Procedure FP1)													
END 1	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625
Diameter 1, in	-0.00120	-0.00090	-0.00080	-0.00050	-0.00030	-0.00020	0.00000	0.00000	0.00000	0.00000	0.00010	0.00030	0.00030
Diameter 2, in (rotated 90°)	0.00120	0.00110	0.00090	0.00080	0.00060	0.00030	0.00020	0.00000	0.00000	-0.00020	-0.00060	-0.00080	-0.00100
Difference between max and min readings, in: 0° = 0.00170 90° = 0.00270													
END 2	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625
Diameter 1, in	-0.00120	-0.00110	-0.00080	-0.00040	-0.00030	-0.00010	0.00000	0.00000	0.00000	0.00010	0.00040	0.00050	0.00060
Diameter 2, in (rotated 90°)	-0.00180	-0.00160	-0.00120	-0.00090	-0.00050	-0.00030	-0.00010	0.00000	0.00010	0.00020	0.00040	0.00070	0.00080
Difference between max and min readings, in: 0° = 0.0018 90° = 0.0028 Maximum difference must be < 0.0020 in. Difference = ± 0.00140 Flatness Tolerance Met? NO													



DIAMETER 1	
End 1:	
Slope of Best Fit Line	0.00086
Angle of Best Fit Line:	0.04911
End 2:	
Slope of Best Fit Line	0.00103
Angle of Best Fit Line:	0.05877
Maximum Angular Difference:	0.00966
Parallelism Tolerance Met? Spherically Seated	NO



DIAMETER 2	
End 1:	
Slope of Best Fit Line	0.00154
Angle of Best Fit Line:	0.08840
End 2:	
Slope of Best Fit Line	0.00157
Angle of Best Fit Line:	0.08987
Maximum Angular Difference:	0.00147
Parallelism Tolerance Met? Spherically Seated	YES

PERPENDICULARITY (Procedure P1)					(Calculated from End Flatness and Parallelism measurements above)	
END 1	Difference, Maximum and Minimum (in.)	Diameter (in.)	Slope	Angle°	Perpendicularity Tolerance Met?	Maximum angle of departure must be $\leq 0.25^\circ$
Diameter 1, in	0.00170	1.987	0.00086	0.049	YES	Perpendicularity Tolerance Met? YES
Diameter 2, in (rotated 90°)	0.00270	1.987	0.00136	0.078	YES	
END 2						
Diameter 1, in	0.00180	1.987	0.00091	0.052	YES	
Diameter 2, in (rotated 90°)	0.00280	1.987	0.00141	0.081	YES	



Client:	WSP USA, Inc.	Test Date:	12/10/2024
Project Name:	Vtrans Jamaica Bridge 42	Tested By:	jss
Project Location:	Jamaica, VT	Checked By:	smd
GTX #:	320233		
Boring ID:	B425	Reliable dial gauge measurements could not be performed on this rock type. Tolerance measurements were performed using a machinist straightedge and feeler gauges to ASTM specifications.	
Sample ID:	Run 2		
Depth (ft):	36.7-37.05		
Visual Description:	See photographs		

BEST EFFORT END FLATNESS TOLERANCES OF ROCK CORE SPECIMENS TO
ASTM D4543

END FLATNESS

END 1

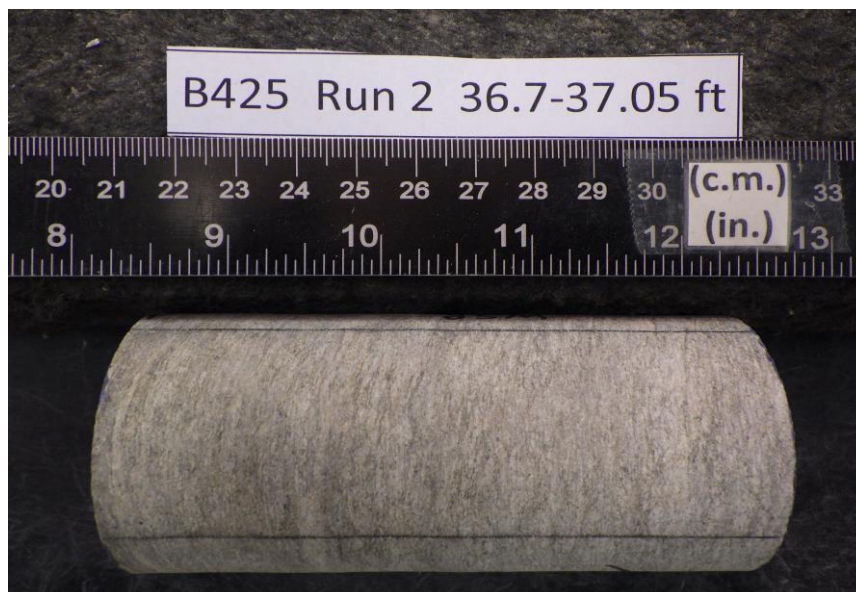
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES

END 2

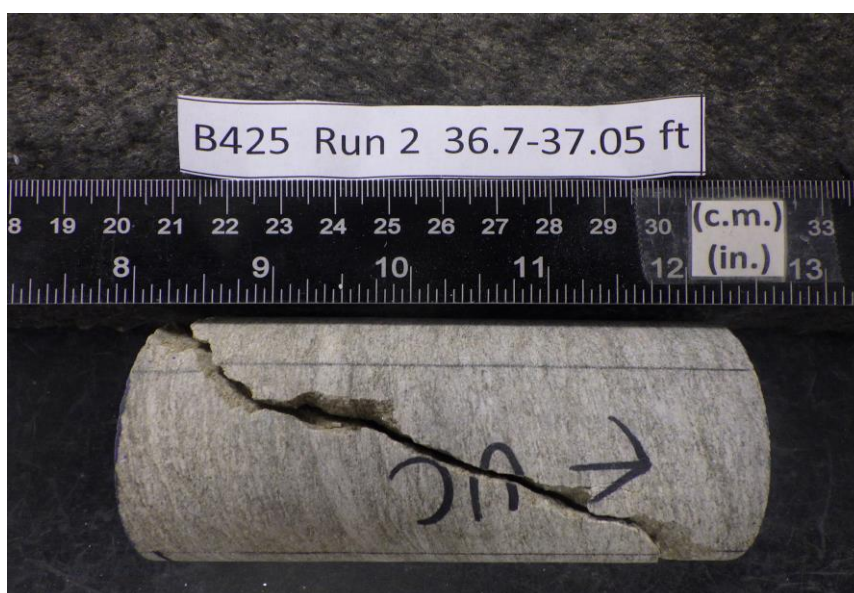
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES

End Flatness Tolerance Met? YES

Client:	WSP USA, Inc.
Project Name:	VTrans Jamaica Bridge 42
Project Location:	Jamaica, VT
GTX #:	320233
Test Date:	12/11/2024
Tested By:	gp
Checked By:	smd
Boring ID:	B425
Sample ID:	Run 2
Depth, ft:	36.7-37.05



After cutting and grinding



After break

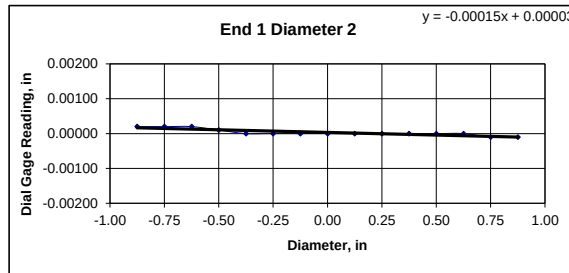
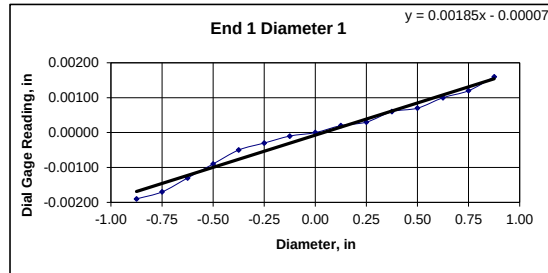


Client:	WSP USA, Inc.	Test Date:	12/10/2024
Project Name:	Vtrans Jamaica Bridge 42	Tested By:	jss
Project Location:	Jamaica, VT	Checked By:	smd
GTx #:	320233		
Boring ID:	B425		
Sample ID:	Run 3		
Depth, ft:	43.6-44.0		
Visual Description:	See photographs		

UNIT WEIGHT DETERMINATION AND DIMENSIONAL AND SHAPE TOLERANCES OF ROCK CORE SPECIMENS BY ASTM D4543

BULK DENSITY				DEVIATION FROM STRAIGHTNESS (Procedure S1)	
	1	2	Average	Maximum gap between side of core and reference surface plate: Is the maximum gap ≤ 0.02 in.? NO	
Specimen Length, in:	4.37	4.37	4.37	Maximum difference must be < 0.020 in. Straightness Tolerance Met? NO	
Specimen Diameter, in:	1.99	1.99	1.99		
Specimen Mass, g:	600.26				
Bulk Density, lb/ft ³	169				
Length to Diameter Ratio:	2.2	Minimum Diameter Tolerance Met? YES	Length to Diameter Ratio Tolerance Met? YES		

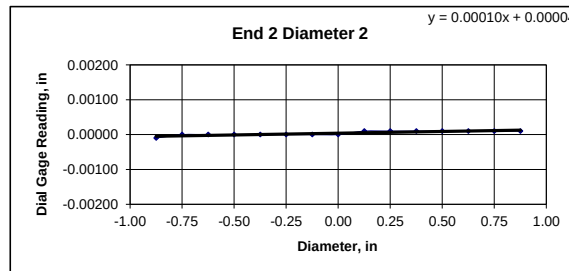
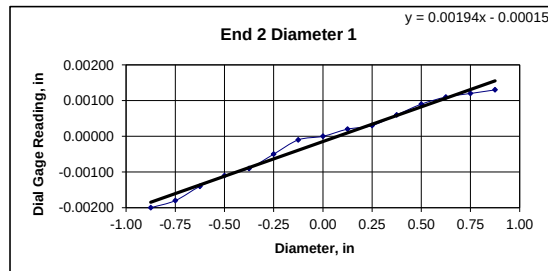
END FLATNESS AND PARALLELISM (Procedure FP1)															
END 1	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750	0.875
Diameter 1, in	-0.00190	-0.00170	-0.00130	-0.00090	-0.00050	-0.00030	-0.00010	0.00000	0.00020	0.00030	0.00060	0.00070	0.00100	0.00120	0.00160
Diameter 2, in (rotated 90°)	0.00020	0.00020	0.00020	0.00010	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	-0.00010	-0.00010
Difference between max and min readings, in: 0° = 0.00350 90° = 0.00030															
END 2	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750	0.875
Diameter 1, in	-0.00200	-0.00180	-0.00140	-0.00110	-0.00090	-0.00050	-0.00010	0.00000	0.00020	0.00030	0.00060	0.00090	0.00110	0.00120	0.00130
Diameter 2, in (rotated 90°)	-0.00010	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00000	0.00010	0.00010	0.00010	0.00010	0.00010	0.00010	0.00010
Difference between max and min readings, in: 0° = 0.0033 90° = 0.0002 Maximum difference must be < 0.0020 in. Difference = ± 0.00175 Flatness Tolerance Met? NO															



DIAMETER 1

End 1:	Slope of Best Fit Line	0.00185
	Angle of Best Fit Line:	0.10575
End 2:	Slope of Best Fit Line	0.00194
	Angle of Best Fit Line:	0.11132
Maximum Angular Difference:		0.00557

Parallelism Tolerance Met? NO
Spherically Seated



DIAMETER 2

End 1:	Slope of Best Fit Line	0.00015
	Angle of Best Fit Line:	0.00868
End 2:	Slope of Best Fit Line	0.00010
	Angle of Best Fit Line:	0.00573
Maximum Angular Difference:		0.00295

Parallelism Tolerance Met? YES
Spherically Seated

PERPENDICULARITY (Procedure P1)						(Calculated from End Flatness and Parallelism measurements above)	
END 1	Difference, Maximum and Minimum (in.)	Diameter (in.)	Slope	Angle°	Perpendicularity Tolerance Met?	Maximum angle of departure must be $\leq 0.25^\circ$	
Diameter 1, in	0.00350	1.987	0.00176	0.101	YES	Perpendicularity Tolerance Met? YES	
Diameter 2, in (rotated 90°)	0.00030	1.987	0.00015	0.009	YES		
END 2							
Diameter 1, in	0.00330	1.987	0.00166	0.095	YES		
Diameter 2, in (rotated 90°)	0.00020	1.987	0.00010	0.006	YES		



Client:	WSP USA, Inc.	Test Date:	12/10/2024
Project Name:	Vtrans Jamaica Bridge 42	Tested By:	jss
Project Location:	Jamaica, VT	Checked By:	smd
GTX #:	320233		
Boring ID:	B425	Reliable dial gauge measurements could not be performed on this rock type. Tolerance measurements were performed using a machinist straightedge and feeler gauges to ASTM specifications.	
Sample ID:	Run 3		
Depth (ft):	43.6-44.0		
Visual Description:	See photographs		

BEST EFFORT END FLATNESS TOLERANCES OF ROCK CORE SPECIMENS TO
ASTM D4543

END FLATNESS

END 1

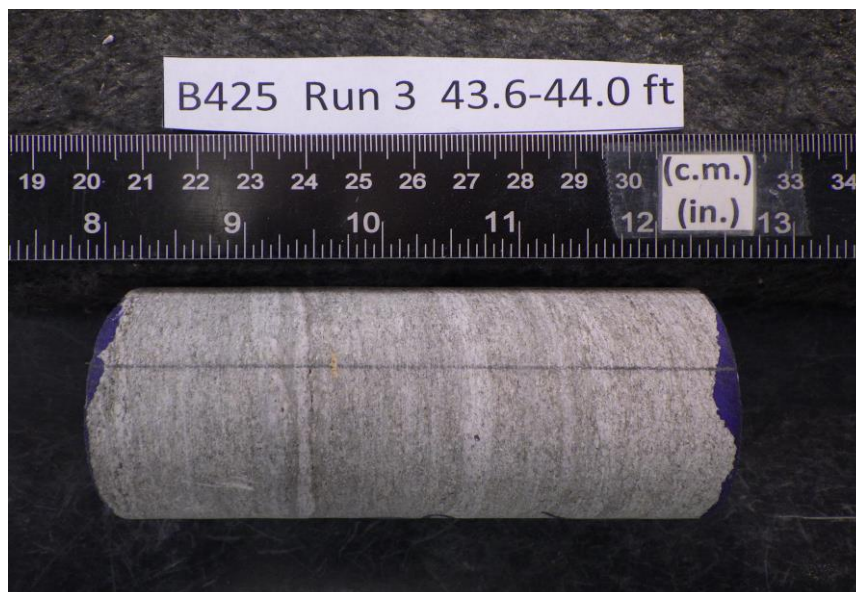
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES

END 2

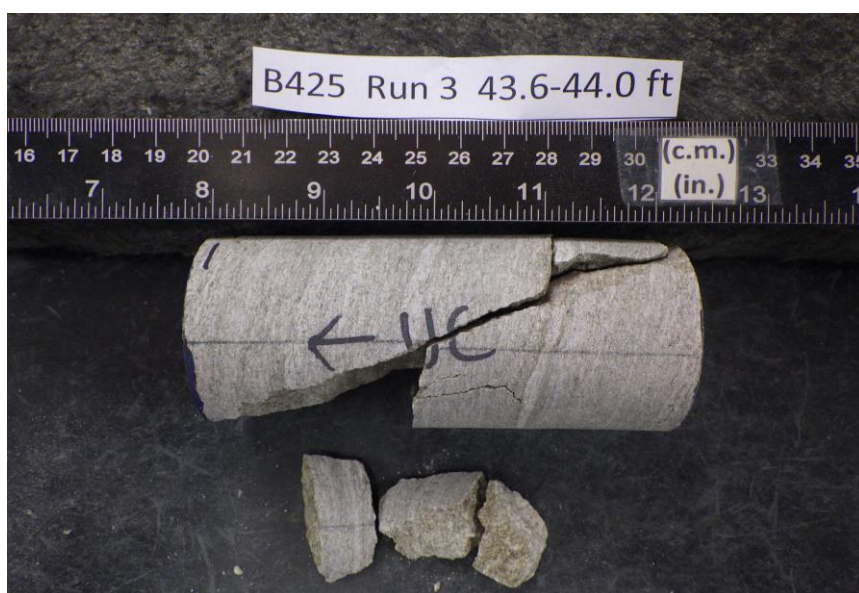
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES

End Flatness Tolerance Met? YES

Client:	WSP USA, Inc.
Project Name:	VTrans Jamaica Bridge 42
Project Location:	Jamaica, VT
GTX #:	320233
Test Date:	12/11/2024
Tested By:	gp
Checked By:	smd
Boring ID:	B425
Sample ID:	Run 3
Depth, ft:	43.6-44.0



After cutting and grinding



After break

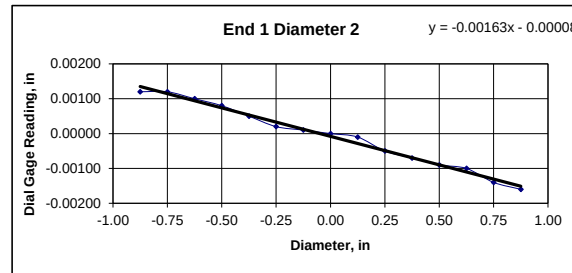
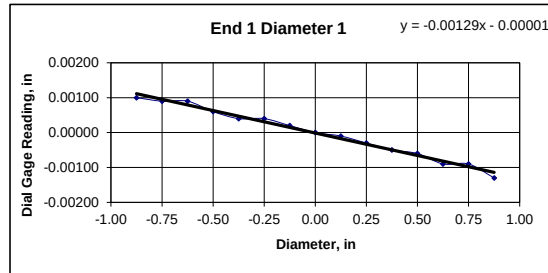


Client:	WSP USA, Inc.	Test Date:	12/10/2024
Project Name:	Vtrans Jamaica Bridge 42	Tested By:	jss
Project Location:	Jamaica, VT	Checked By:	smd
GTX #:	320233		
Boring ID:	B545		
Sample ID:	Run 1		
Depth, ft:	38.54-38.91		
Visual Description:	See photographs		

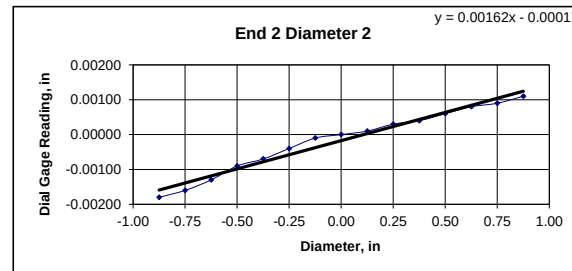
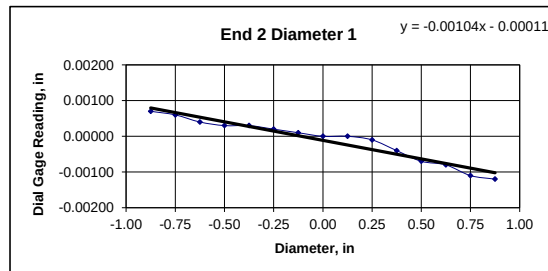
UNIT WEIGHT DETERMINATION AND DIMENSIONAL AND SHAPE TOLERANCES OF ROCK CORE SPECIMENS BY ASTM D4543

BULK DENSITY				DEVIATION FROM STRAIGHTNESS (Procedure S1)	
	1	2	Average	Maximum gap between side of core and reference surface plate: Is the maximum gap ≤ 0.02 in.? NO	
Specimen Length, in:	4.19	4.20	4.20	Maximum difference must be < 0.020 in.	
Specimen Diameter, in:	1.99	1.99	1.99	Straightness Tolerance Met? NO	
Specimen Mass, g:	566.65				
Bulk Density, lb/ft ³ :	166				
Length to Diameter Ratio:	2.1				
		Minimum Diameter Tolerance Met?	YES		
		Length to Diameter Ratio Tolerance Met?	YES		

END FLATNESS AND PARALLELISM (Procedure FP1)														
END 1	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750
Diameter 1, in	0.00100	0.00090	0.00090	0.00060	0.00040	0.00040	0.00020	0.00000	-0.00010	-0.00030	-0.00050	-0.00060	-0.00090	-0.00130
Diameter 2, in (rotated 90°)	0.00120	0.00120	0.00100	0.00080	0.00050	0.00020	0.00010	0.00000	-0.00010	-0.00050	-0.00070	-0.00090	-0.00100	-0.00140
Difference between max and min readings, in:														
0° = 0.00230 90° = 0.00280														
END 2	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625	0.750
Diameter 1, in	0.00070	0.00060	0.00040	0.00030	0.00030	0.00020	0.00010	0.00000	0.00000	-0.00010	-0.00040	-0.00070	-0.00080	-0.00110
Diameter 2, in (rotated 90°)	-0.00180	-0.00160	-0.00130	-0.00090	-0.00070	-0.00040	-0.00010	0.00000	0.00010	0.00030	0.00040	0.00060	0.00080	0.00090
Difference between max and min readings, in:														
0° = 0.0019 90° = 0.0029														
Maximum difference must be < 0.0020 in. Difference = ± 0.00145														
Flatness Tolerance Met? NO														



DIAMETER 1	
End 1:	
Slope of Best Fit Line	0.00129
Angle of Best Fit Line:	0.07383
End 2:	
Slope of Best Fit Line	0.00104
Angle of Best Fit Line:	0.05942
Maximum Angular Difference:	0.01441
Parallelism Tolerance Met?	NO
Spherically Seated	



DIAMETER 2	
End 1:	
Slope of Best Fit Line	0.00163
Angle of Best Fit Line:	0.09364
End 2:	
Slope of Best Fit Line	0.00162
Angle of Best Fit Line:	0.09282
Maximum Angular Difference:	0.00082
Parallelism Tolerance Met?	YES
Spherically Seated	

PERPENDICULARITY (Procedure P1)						(Calculated from End Flatness and Parallelism measurements above)	
END 1		Difference, Maximum and Minimum (in.)	Diameter (in.)	Slope	Angle°	Perpendicularity Tolerance Met?	Maximum angle of departure must be $\leq 0.25^\circ$
Diameter 1, in		0.00230	1.987	0.00116	0.066	YES	
Diameter 2, in (rotated 90°)		0.00280	1.987	0.00141	0.081	YES	Perpendicularity Tolerance Met? YES
END 2							
Diameter 1, in		0.00190	1.987	0.00096	0.055	YES	
Diameter 2, in (rotated 90°)		0.00290	1.987	0.00146	0.084	YES	



Client:	WSP USA, Inc.	Test Date:	12/10/2024
Project Name:	Vtrans Jamaica Bridge 42	Tested By:	jss
Project Location:	Jamaica, VT	Checked By:	smd
GTX #:	320233		
Boring ID:	B545	Reliable dial gauge measurements could not be performed on this rock type. Tolerance measurements were performed using a machinist straightedge and feeler gauges to ASTM specifications.	
Sample ID:	Run 1		
Depth (ft):	38.54-38.91		
Visual Description:	See photographs		

BEST EFFORT END FLATNESS TOLERANCES OF ROCK CORE SPECIMENS TO
ASTM D4543

END FLATNESS

END 1

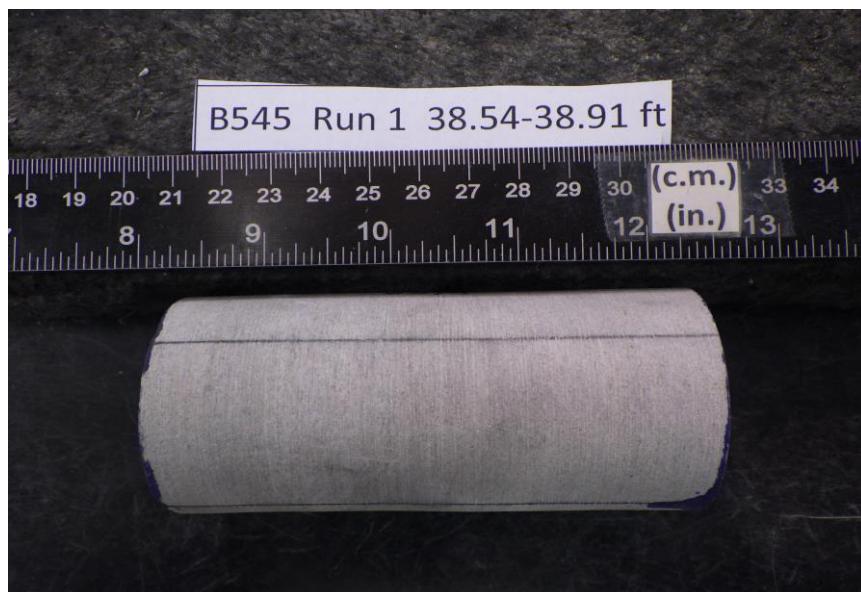
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES

END 2

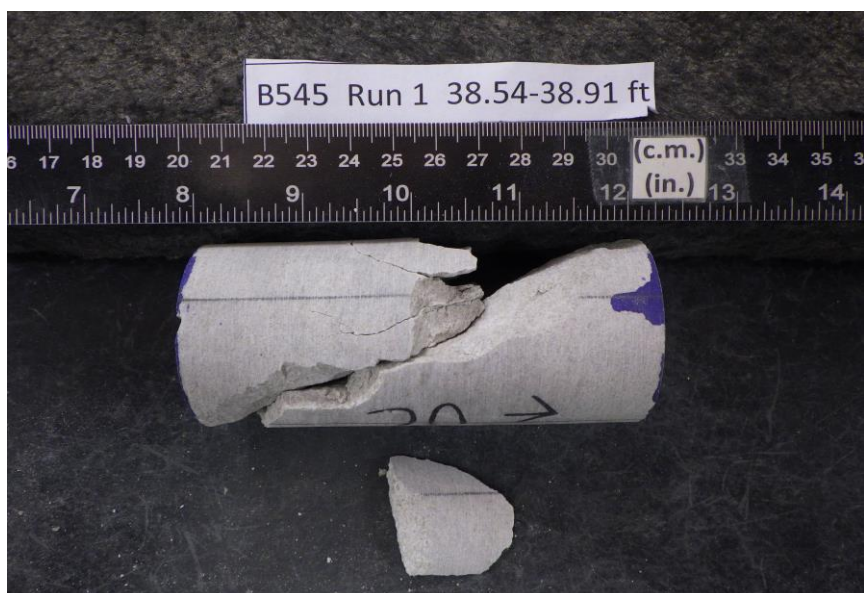
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES

End Flatness Tolerance Met? YES

Client:	WSP USA, Inc.
Project Name:	VTrans Jamaica Bridge 42
Project Location:	Jamaica, VT
GTX #:	320233
Test Date:	12/11/2024
Tested By:	gp
Checked By:	smd
Boring ID:	B545
Sample ID:	Run 1
Depth, ft:	38.54-38.91



After cutting and grinding



After break

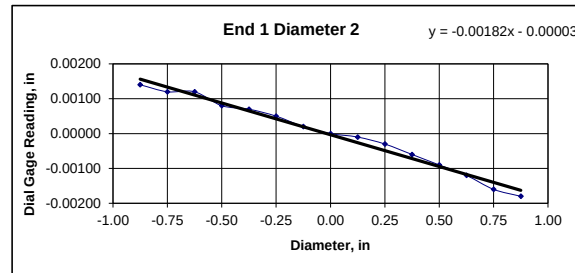
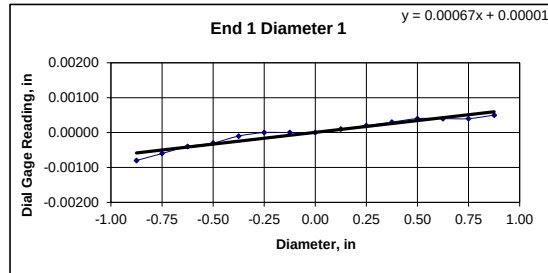


Client:	WSP USA, Inc.	Test Date:	12/10/2024
Project Name:	Vtrans Jamaica Bridge 42	Tested By:	jss
Project Location:	Jamaica, VT	Checked By:	smd
GTx #:	320233		
Boring ID:	B545		
Sample ID:	Run 2		
Depth, ft:	44.23-44.61		
Visual Description:	See photographs		

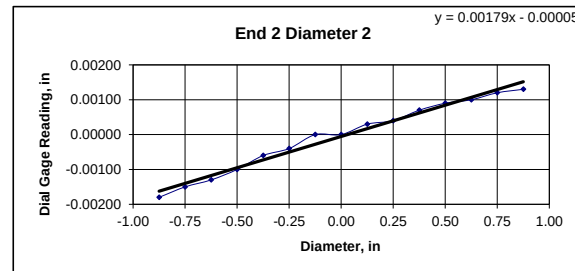
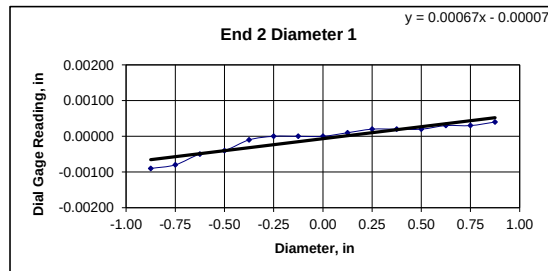
UNIT WEIGHT DETERMINATION AND DIMENSIONAL AND SHAPE TOLERANCES OF ROCK CORE SPECIMENS BY ASTM D4543

BULK DENSITY				DEVIATION FROM STRAIGHTNESS (Procedure S1)	
	1	2	Average	Maximum gap between side of core and reference surface plate: Is the maximum gap ≤ 0.02 in.? NO	
Specimen Length, in:	4.39	4.39	4.39	Maximum difference must be < 0.020 in.	
Specimen Diameter, in:	1.99	1.99	1.99	Straightness Tolerance Met? NO	
Specimen Mass, g:	595.98				
Bulk Density, lb/ft ³ :	167				
Length to Diameter Ratio:	2.2	Minimum Diameter Tolerance Met? YES	Length to Diameter Ratio Tolerance Met? YES		

END FLATNESS AND PARALLELISM (Procedure FP1)													
END 1	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625
Diameter 1, in	-0.00080	-0.00060	-0.00040	-0.00030	-0.00010	0.00000	0.00000	0.00000	0.00010	0.00020	0.00030	0.00040	0.00050
Diameter 2, in (rotated 90°)	0.00140	0.00120	0.00120	0.00080	0.00070	0.00050	0.00020	0.00000	-0.00010	-0.00030	-0.00060	-0.00090	-0.00120
Difference between max and min readings, in:													
0° = 0.00130 90° = 0.00320													
END 2	-0.875	-0.750	-0.625	-0.500	-0.375	-0.250	-0.125	0.000	0.125	0.250	0.375	0.500	0.625
Diameter 1, in	-0.00090	-0.00080	-0.00050	-0.00040	-0.00010	0.00000	0.00000	0.00000	0.00010	0.00020	0.00020	0.00030	0.00040
Diameter 2, in (rotated 90°)	-0.00180	-0.00150	-0.00130	-0.00100	-0.00060	-0.00040	0.00000	0.00000	0.00030	0.00040	0.00070	0.00090	0.00100
Difference between max and min readings, in:													
0° = 0.0013 90° = 0.0031													
Maximum difference must be < 0.0020 in. Difference = ± 0.00160													
Flatness Tolerance Met? NO													



DIAMETER 1	
End 1:	
Slope of Best Fit Line	0.00067
Angle of Best Fit Line:	0.03863
End 2:	
Slope of Best Fit Line	0.00067
Angle of Best Fit Line:	0.03847
Maximum Angular Difference:	0.00016
Parallelism Tolerance Met? Spherically Seated	YES



DIAMETER 2	
End 1:	
Slope of Best Fit Line	0.00182
Angle of Best Fit Line:	0.10444
End 2:	
Slope of Best Fit Line	0.00179
Angle of Best Fit Line:	0.10280
Maximum Angular Difference:	0.00164
Parallelism Tolerance Met? Spherically Seated	YES

PERPENDICULARITY (Procedure P1)						Maximum angle of departure must be $\leq 0.25^\circ$	
END 1	Difference, Maximum and Minimum (in.)	Diameter (in.)	Slope	Angle°	Perpendicularity Tolerance Met?		
Diameter 1, in	0.00130	1.986	0.00065	0.038	YES		
Diameter 2, in (rotated 90°)	0.00320	1.986	0.00161	0.092	YES	Perpendicularity Tolerance Met? YES	
END 2							
Diameter 1, in	0.00130	1.986	0.00065	0.038	YES		
Diameter 2, in (rotated 90°)	0.00310	1.986	0.00156	0.089	YES		



Client:	WSP USA, Inc.	Test Date:	12/10/2024
Project Name:	Vtrans Jamaica Bridge 42	Tested By:	jss
Project Location:	Jamaica, VT	Checked By:	smd
GTX #:	320233		
Boring ID:	B545	Reliable dial gauge measurements could not be performed on this rock type. Tolerance measurements were performed using a machinist straightedge and feeler gauges to ASTM specifications.	
Sample ID:	Run 2		
Depth (ft):	44.23-44.61		
Visual Description:	See photographs		

BEST EFFORT END FLATNESS TOLERANCES OF ROCK CORE SPECIMENS TO
ASTM D4543

END FLATNESS

END 1

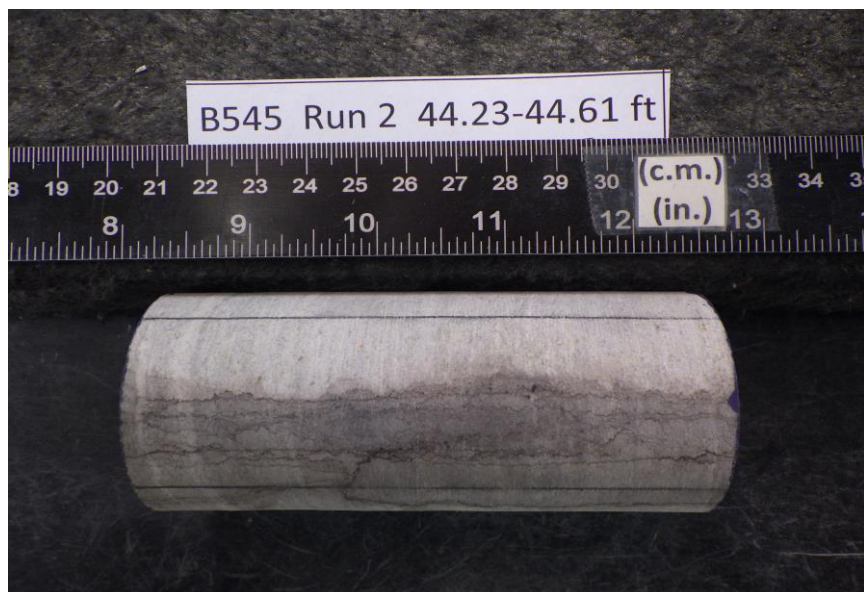
Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES

END 2

Diameter 1	Is the maximum gap $\leq \pm 0.001$ in.?	YES
Diameter 2 (rotated 90°)	Is the maximum gap $\leq \pm 0.001$ in.?	YES

End Flatness Tolerance Met? YES

Client:	WSP USA, Inc.
Project Name:	VTrans Jamaica Bridge 42
Project Location:	Jamaica, VT
GTX #:	320233
Test Date:	12/11/2024
Tested By:	gp
Checked By:	smd
Boring ID:	B545
Sample ID:	Run 2
Depth, ft:	44.23-44.61



After cutting and grinding



After break